

## **Investigation of the nanocomposite material $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + \text{ZrO}_2$ as a resistive superconducting fault-current limiter.**

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**Abstract.** The effects of nanoscale inclusions  $\text{ZrO}_2$  as the second component of the composites on the magnetic and transport properties of superconducting polycrystals  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$  are studied. Samples of  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$  with different (0.5, 4, 8 и 12 wt.%) contents of  $\text{ZrO}_2$  nanoparticles were synthesized. Measurements of the magnetization in the field range up to 5 T and recalculation using the Bean model showed that JC in the case of composite samples is larger than the initial one in the entire range of the magnetic field. The results of experimental studies of switching superconducting fault-current limiter in AC voltage networks based on high-temperature superconductors (HTSC) of the 2<sup>nd</sup> generation are given. The stand contains a series-connected HTSC module and a high-speed current switch with a shutdown time of 9 ms. The high efficiency of samples from the nanocomposite material  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + \text{ZrO}_2$  as a resistive superconducting fault-current limiter was shown.

**Keywords:** YBCO ceramics, critical current, resistive superconducting fault-current limiter.

**Introduction.** One of the promising ways of limiting fault currents (FC) could be the creation of current-limiting devices based on high-temperature superconductors (HTSC) of the 2<sup>nd</sup> generation [1]. Such materials, in comparison with previous-generation superconductors, are characterized by reduced metal content (small thickness of the substrate and stabilizer), additional heat removal, a higher critical current value and a high resistance to emergency currents in a normal state. In normal operation, the device has practically no influence on the mode of the system, while in emergency operation, it introduces the resistance, necessary to limit the fault current to the required level, into the network.

Based on design features, two basic concepts of a superconducting fault current limiter (SFCL) can be distinguished: resistive and inductive. Other schematic solutions are based on

these concepts [2]. In the case of inductive design, the magnetic coupling between the superconducting element and the winding is carried out through a three-core magnetic conductor [3]. For example, the ABB company developed three-phase current limiter (1.2 MVA) with a cylindrical screen consisting of 16 rings which were made from the superconducting ceramics Bi-2212, which was tested and operated during the year [4]. The operation of an inductive current limiter is concerned with the presence of magnetic stray fields, which can adversely affect the use of a metal cryostat and increase power loss.

The resistive design of a SFCL is based on the nonlinearity of the superconductor resistance and it could use massive elements or coils [5]. When superconducting coils are used as superconducting elements, they are arranged in such a way to make the total inductance of the limiter possibly minimal [6]. A resistive superconducting current limiter contains a HTSC module placed in a cryostat with liquid or supercooled nitrogen, acting as a cooling agent, and high-voltage current inputs of a special design. The basic disadvantage of a resistive SFCL is considerable heat generation, the presence of magnetic stray fields, overheating during a short circuit, and a relatively long response time.

The paper [7] describes the development of composite material based on the  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$  granular superconductor and CuO electric arc nanopowders [8–12]. The addition of CuO nanopowders improves the quality of the sintered composites, with significant increase in the critical current density, as well as a peak effect in the region of strong magnetic fields [13]. Changing the concentration of CuO nanopowders make it possible to achieve a smooth regulation of the critical current density and a decrease in the transition time to the normal state. At the same time, there is evidence [14, 15] that  $\text{ZrO}_2$  in the HTSC / nano  $\text{ZrO}_2$  composite leads to an impressive increase in the critical current and to a smaller attenuation of the magnetic field.

This paper presents the results of measuring the magnetic and transport characteristics of the obtained nanocomposite material  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + \text{ZrO}_2$ , parameters of a polycrystalline (ceramic) HTSC device connected in accordance with the series subcircuit in the current limiting mode to 1200 A during the first half-wave of an alternating current. Theoretically, such a ballast resistance at a transport current less than the critical ( $J_c$ ) is equal to zero and, when an emergency situation occurs, accompanied by an increase in current above  $J_c$ , it “switches on” into the circuit and limits the current to a given value. In the practical implementation of such a limiter, it is necessary to overcome a number of technical challenges, among them are the problem of contacts in HTSC, the problem of heat removal from the HTSC protection element in the short circuit protection mode (when the HTSC

remains the only consumer) and the resulting task of negotiating the HTSC element according to the voltage drop in the resistive state with the voltage of the protected circuit, which determines its geometrical dimensions and the power developed in a unit of volume.

**Experimental.** The samples for measurements were made by pressing and sintering (temp. 930 °C) the prepared HTSC powder  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$  with  $\text{ZrO}_2$  nanoparticles coated on the surface. The preparation of composites  $\text{Y}_1\text{Ba}_2\text{Cu}_3\text{O}_{7-\delta} + x\text{ZrO}_2$  was carried out on a device described in detail in paper [16]. A distinctive feature was the use as a cathode for spraying zirconium of technical purity. The remaining parameters are further described in paper [15]. During the experiment, the samples with 0.5, 4, 8 и 12 wt.%  $\text{ZrO}_2$  were used. The samples were protected on the top with a layer of silver with a thickness of about 2 microns without a stabilizing copper shell, which is better suited for use in resistive superconducting current limiters, since they have the highest resistance in a normal non-superconducting state. The typical sample size was  $2 \times 7 \times 44$  mm. To increase the area to the maximum possible, the current contacts were covered with In – Ga eutectic. The assembled unit was placed in a bath with liquid nitrogen. The studies were conducted on a low-voltage testing equipment, which contained a transformer with an output voltage  $U_0 = 20$  V (rms value), a network key  $K_1$  with an electromagnetic drive, a load resistance  $R_0 = 0.2 \Omega$ , and a control system (Fig. 1). A chain with the connected in series thyristor key  $VT$  and the additional resistance  $R_1$  was wired parallel to the  $R_0$  resistance. The key  $VT$  was used to simulate the occurrence of fault current, the amplitude of which was regulated by changing the resistance  $R_1$ . The test samples  $R_{\text{HTSC}}$  and switch  $K_2$  were connected to the output of the transformer before the load resistance  $R_0$ . During the experiments, the HTSC samples were immersed in a Dewar vessel filled with liquid nitrogen.

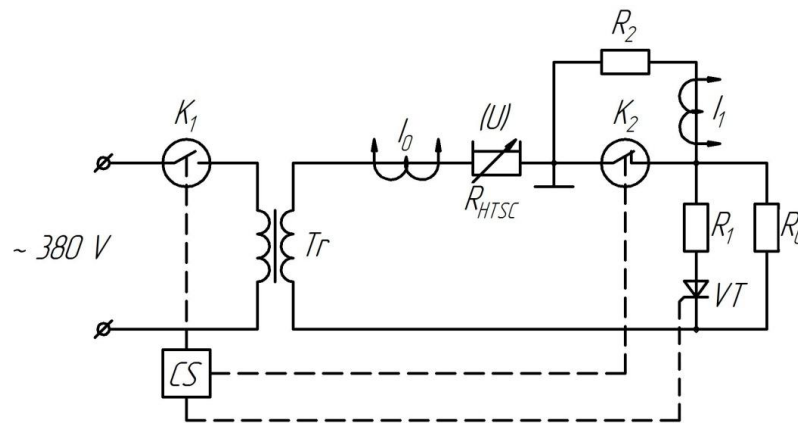


Figure 1. Electrical circuit of the testing equipment ( $K_1$  – network key,  $VT$  – load generation key,  $K_2$  – turn-off key,  $CS$  – control system,  $R_0$  – load resistance,  $R_1$  – additional resistance,  $R_2$  – shunt resistance)

The control system (CS) generated signals with an adjustable turn-on delay  $K_1$  at the moment of circuit voltage maximum, turn-on  $V_T$  to generate a fault current approximately one period after the start of the load current flow, and turn-off  $K_2$  at the end of the first half-wave of the current. The expected amplitude of the first half-wave of the fault current was 4700 A.

To study the recovery mode of the superconducting element of the HTSC after the current was turned off by the  $K_2$  switch, it was shunted by resistance  $R_2$ . The total duration of current flow in the HTSC element was about 300 ms.

The inherent resistance of the low-voltage network in the fault mode was lower (less than 15 mOhm) compared with the resistance of HTSC elements after the transition to the normal state. Therefore, almost all the circuit voltage was applied to HTSC. Such conditions are close to the actual conditions of current limitation in AC networks with a given voltage. The change in the parameters of the current limitation was regulated by changing the additives of  $\text{ZrO}_2$  nanodispersed powder.

For each sample, oscillographic testing of current and voltage was performed. The limited current  $i_{\text{lim}}$  was measured by a galvanically isolated sensor with a sensitivity of 2560 A/V. The electrical signals were recorded using P6139A testers on a Tektronix DPO 4034 oscillograph, and then they were saved and processed on a personal computer. While being processed on a computer, the inductive component of the voltage drop on the HTSC element was subtracted from the measurement data.

The magnetic measurements were carried out with the MPMS-XL5 unit. Debye X-ray patterns were recorded on the D8 ADVANCE diffractometer (Bruker AXS) in  $\text{CuK}\alpha$  monochromatic radiation. The measurements of the isothermal dependences of the magnetization on the magnetic field were carried out at a temperature of 77 K. The critical current density of the samples was estimated from the magnetic hysteresis loop using the extended critical state model [17].

**Results.** Figure 2a shows the diffraction patterns of the obtained  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + x\text{ZrO}_2$  composites ( $x = 0.5, 4, 8, \text{ and } 12 \text{ wt.}\%$ ) at room temperature. An analysis of the diffraction pattern showed that all samples crystallize in the orthorhombic phase with the space group Pmmm. The lattice parameters and other set parameters of all samples are listed in Table 1. All structural parameters, such as lattice parameters, orthorhombicity, unit cell volume, remain unchanged.

The presence of  $\text{ZrO}_2$  in the YBCO matrix is evident due to the appearance of additional peaks in the diffraction pattern, the intensity of which increases with increasing  $\text{ZrO}_2$

concentration in YBCO. Monoclinic ( $2\theta = 28.20, 31.20, 35$ ,  $hkl$ :  $(-111)$ ,  $(111)$ ,  $(002)$ ) and tetragonal ( $2\theta = 30.02, 49.8$ ,  $hkl$ :  $(101)$ ,  $(112)$ )  $\text{ZrO}_2$  phase nanoparticles. Since the transport properties strongly depend on the characteristic features of the microstructure, it becomes important to investigate the effect of adding  $\text{ZrO}_2$  on the microstructure of YBCO. Figure 2b and 2c shows the SEM micrograph of the obtained  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + x\text{ZrO}_2$  composite. The nanopowder is evenly distributed over the surface of YBCO particles and, moreover, it fills the intergranular space and pores, which can act as a catalyst for improving the quality of the structure at the grain boundaries [18]. This forces the grain to behave in a consistent manner and introduces significant changes in mechanical and transport measurements. This observation is consistent with measurements of magnetization.

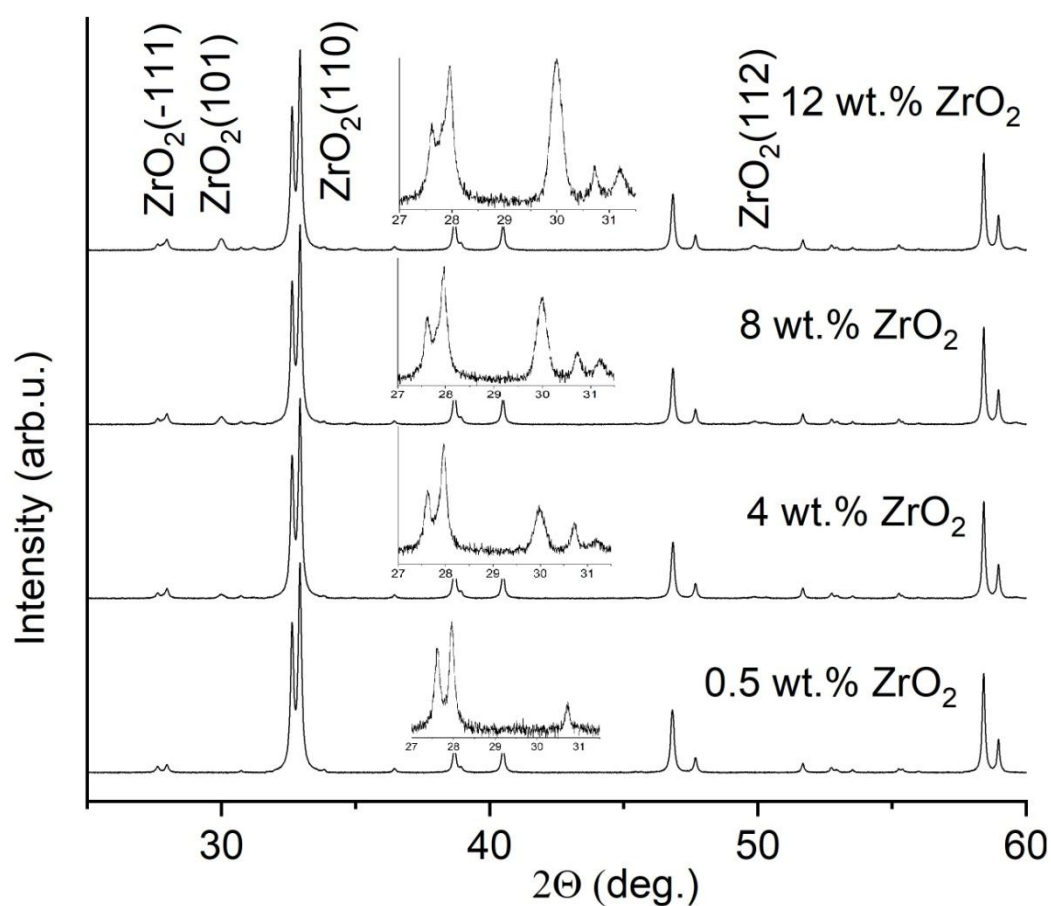


Figure 2a. Diffraction patterns of the composites obtained  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + x\text{ZrO}_2$  ( $x = 0.5, 4, 8, 12$  wt.%)

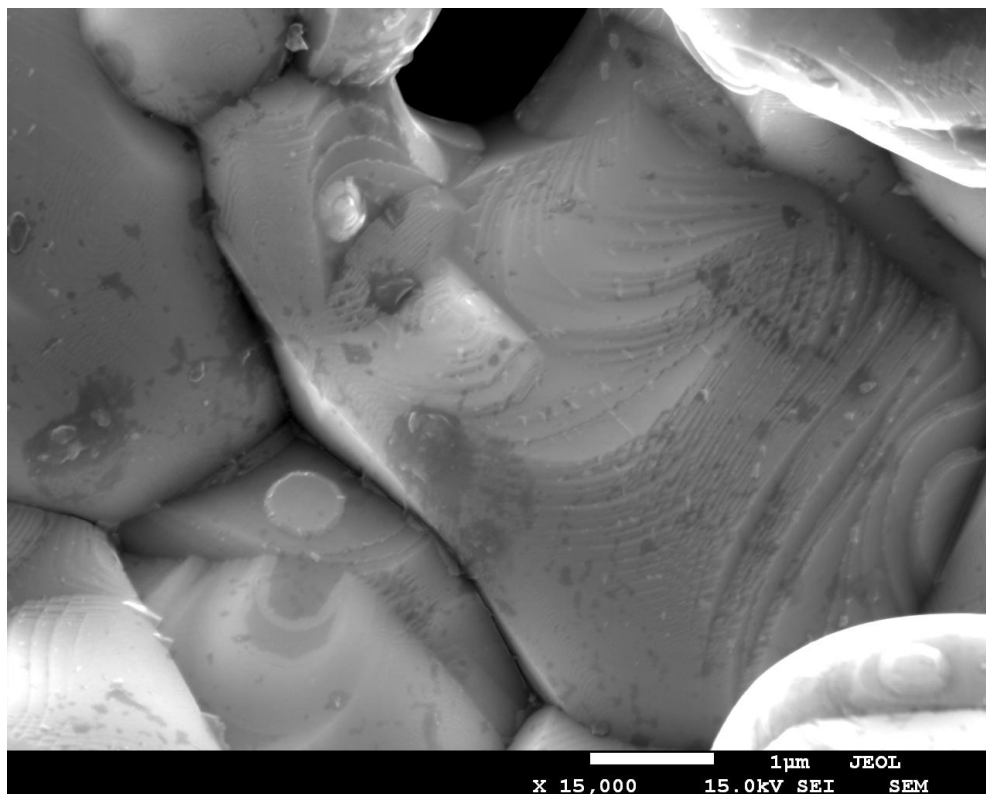


Figure 2b. SEM photomicrograph of the obtained composite  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + 0.5 \text{ wt.}\% \text{ ZrO}_2$

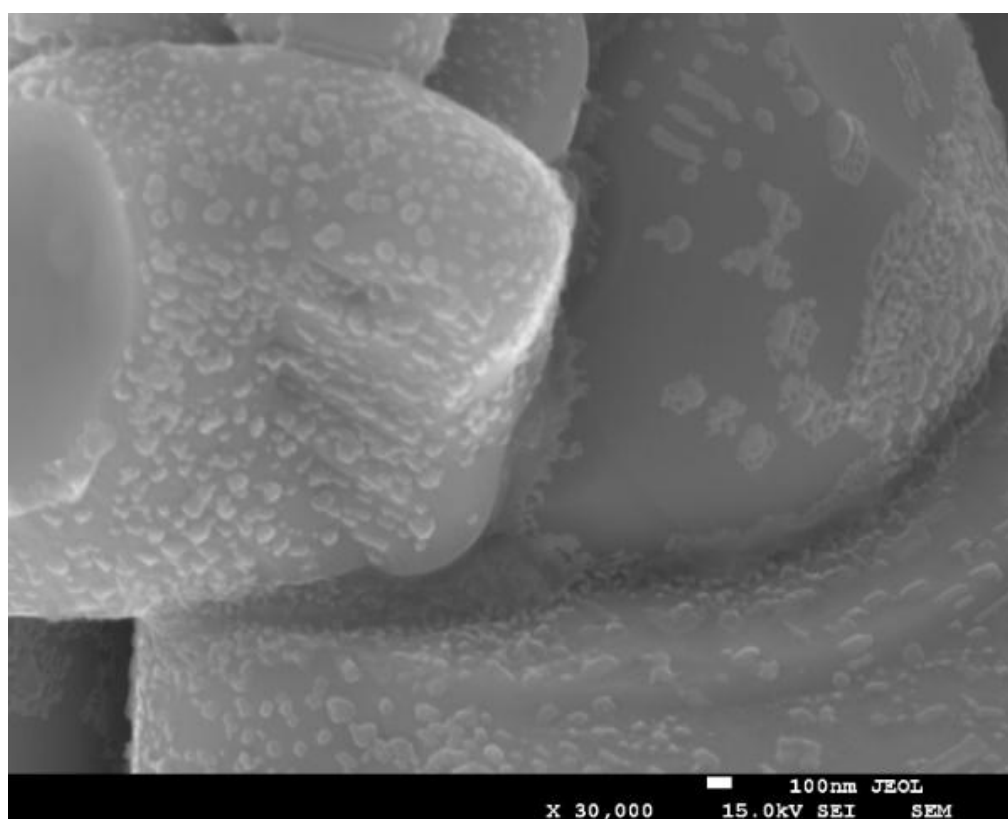


Figure 2c. SEM photomicrograph of the obtained composite  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + 12 \text{ wt.}\% \text{ ZrO}_2$

Table 1. The lattice parameters and the volume of the YBCO cell in the composite.

Sample	$a(\text{\AA})$	$b(\text{\AA})$	$c(\text{\AA})$	Vol.( $\text{\AA}^3$ )
YBCO	3.825	3.888	11.695	173.923
YBCO+0.5 wt.% $\text{ZrO}_2$	3.828	3.890	11.688	174.045
YBCO+4 wt.% $\text{ZrO}_2$	3.827	3.889	11.687	173.940
YBCO+8 wt.% $\text{ZrO}_2$	3.828	3.889	11.689	174.015
YBCO+12 wt. % $\text{ZrO}_2$	3.827	3.885	11.681	173.672

On SEM micrographs, it is also seen that  $\text{ZrO}_2$  does not react with YBCO to form a new phase, but remains as an adhesive material at the grain boundaries, thus making YBCO more attractive for technological applications. Additionally, X-ray phase analysis did not reveal the presence of products of interaction of  $\text{ZrO}_2$  nanoparticles with the HTSC matrix. To study the effect of  $\text{ZrO}_2$  on the temperature of the superconducting transition ( $T_c$ ) YBCO, the change in electrical resistivity as a function of temperature was studied. The data are normalized per unit at 300 K, and the change in the normalized specific resistance of composite samples with temperature is shown in Figure 3. All samples show a superconducting transition of about 90 K, but the transition broadening is greater in the case of composite samples than the original ones. This suggests that the broadening of the transition is apparently due to an increase in the concentration of nano- $\text{ZrO}_2$  in the YBCO matrix. The superconducting transition temperature  $T_c$  practically did not change with the addition of  $\text{ZrO}_2$  in YBCO. This is an important result, since there are examples in the literature when the introduction of the secondary phase leads to an undesirable decrease in the transition temperature [19]. Although  $\text{ZrO}_2$  is a dielectric material, the resistivity of the normal state (electrical resistivity of composite  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + x\text{ZrO}_2$  at 300 K  $\rho=1150\pm20 \mu\Omega\cdot\text{cm}$ ) does not increase with the addition of  $\text{ZrO}_2$ , as one would expect.

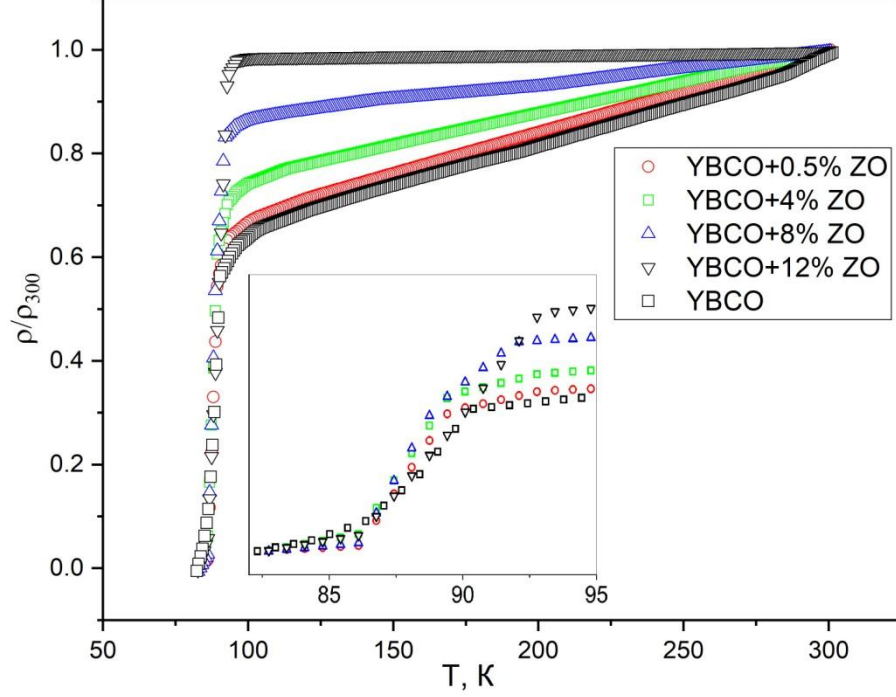


Figure 3. Temperature-dependent normalized resistivity,  $\rho/\rho_{300}$  composites  $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta} + x\text{ZrO}_2$  ( $x = 0.5, 4, 8, 12$  wt.%).

The critical current density strongly depends on the boundary region of the grains and the nature of the cohesion of the grains in  $J_C$  is expected. In order to establish and quantify the change in  $J_C$ , isothermal magnetization measurements were made, and these results are shown in Figure 4a. The measurements were carried out in a wide magnetic field range up to 5T and at a temperature of 5K, where it is assumed that there is no flux creep. The applied magnetic field is set parallel to the long axis of the measured sample, which ensures maximum area and helps to avoid demagnetization. Obviously, as the field increases from 0 to  $H_{CI}$ , the corresponding magnetization also increases in the opposite direction in accordance with the Meissner effect.

As soon as the applied field exceeds  $H_{CI}$ , the magnetic flux begins to penetrate into the sample, leading to the formation of Abrikosov vortices. The density of the magnetic flux lines (normal nuclei) is determined by the equilibrium between the decrease in free energy and mutual repulsion between the vortices. In an increasing magnetic field, normal nuclei are packaged closer to each other, so the average flux density increases in the material, and the magnetization decreases. It was found that the decrease in magnetization is less in the case of a composite sample compared to the original sample [20]. The magnetic flux lines in the mixed state of any superconductor can be fixed by various interactions, such as impurities,



residual stresses, point defects, expanded defects and secondary phases, etc. Thus, the introduction of  $\text{ZrO}_2$  as a secondary phase in YBCO leads to pinning lines magnetic flux, which leads to a smaller decrease in magnetization compared to the original outside of  $H_{C1}$ . In addition, pinning the magnetic flux lines by introducing a secondary phase leads to irreversibility of the magnetization, thereby enhancing  $J_C$ . Using the Bean's critical state model [17], the critical current density ( $J_C$ ) of composite samples is derived from the width of the M-H loop and are presented in Figure 4b.

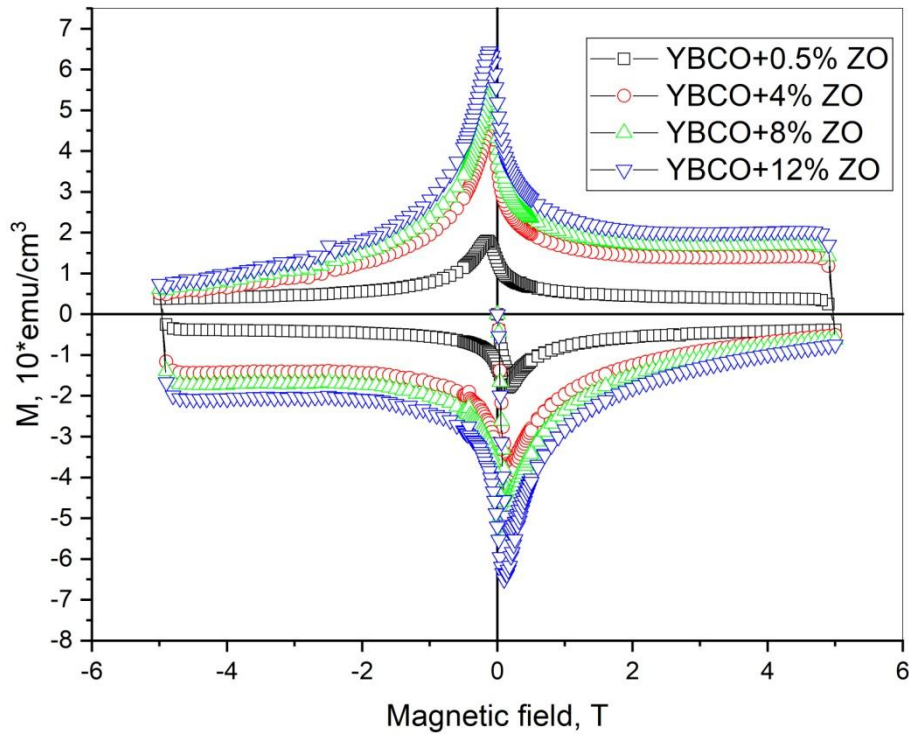


Figure 4a. Isothermal hysteresis loops for magnetization of YBCO +  $x\text{ZrO}_2$  samples ( $x = 0.5$ , 4, 8, and 12 wt.%) at 5 K

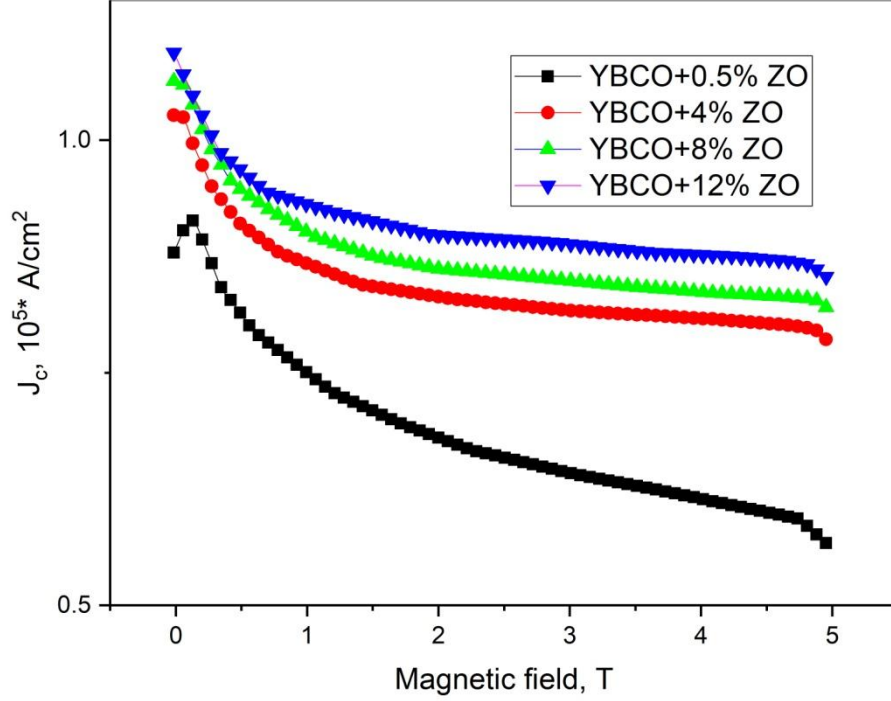


Figure 4b.  $J_C$  curves depending on the applied magnetic field for samples YBCO +  $x\text{ZrO}_2$  ( $x = 0.5, 4, 8$ , and  $12$  wt.%) at  $5$  K

The critical current density depending on the applied magnetic field for different composite samples is shown in Figure 4b. It was found that  $J_C$  in the case of composite samples is larger than the initial one in the entire range of the magnetic field. The peak  $J_C$  value is  $6.7 \times 10^4$  A/cm<sup>2</sup> for the initial sample and  $1.8 \times 10^5$  A/cm<sup>2</sup> for YBCO +  $8$  wt.%  $\text{ZrO}_2$ . Thus, for a given concentration of  $\text{ZrO}_2$ ,  $J_C$  is increased by a factor of  $3$ . In addition,  $J_C$  at  $50$  kOe is almost  $10$  times more than the original.

The gain of  $J_C$  is explained by pinning the magnetic flux of  $\text{ZrO}_2$  in YBCO. Zr-doping in YBCO has been studied extensively since the first work by J. L. Macmanus-Driscoll et al [21]. The primary effect of the “Zr” doping is the formation of  $\text{BaZrO}_3$  nanostructures (nanoparticles, nanorods, etc) that serve as strong pinning centers of magnetic vortices. The most favorable growth of  $\text{ZrO}_2$  in YBCO occurs in the form of islands and creates columnar defects in YBCO, which are responsible for increasing the critical current density [13]. The reason for this enhancement of pinning may be due to the fact that  $\text{ZrO}_2$ , in addition to increasing the binding of grains by filling in cracks and voids, also creates artificial pinning centers that prevent the movement of magnetic flux lines. These artificial pinning centers are responsible for enhancing  $J_C$  even at high applied magnetic fields, which makes YBCO interesting for technological applications. One of the most convenient ways to increase  $J_C$

superconducting materials is to create extended defects that act as artificial pinning centers, other than those that occur naturally. The effect of pinning centers is better when their dimensions are of the order of the coherence length. In this case, the most favorable growth of  $\text{ZrO}_2$  in YBCO has the appearance of islands and creates columnar defects in YBCO, which are responsible for increasing the critical current density.

The results of studying the produced composites and their application as a resistive current limiter are shown in Figure 5. After the contactor  $K_I$  was turned on, a load current began to flow in the circuit (the first one and a half periods), the amplitude of which (155 A) was about 2 times less than that of the critical current  $I_c$ . To demonstrate the effect of limiting the fault current, oscillographic testing of the current was carried out with simulation of fault current appearance without an HTSC element. In this case, a current  $i_f$  with an aperiodic component of 4700 A amplitude flowed in the circuit. With HTSC present, the current in the circuit was limited due to a nonlinear increase in the resistance of the superconductor after its transition to the normal (non-superconducting) state. The limiting current  $I_{max}$  was determined by the degree of HTSC heating during the current half-wave.

Figure 5a shows the current-limiting mode for the HTSC sample without addition of nano-dispersed  $\text{ZrO}_2$  powder at  $R_1 = 0$ . Figure 5a was obtained by superimposing oscillograms of the limiting current  $i_{lim}$  and voltage on the HTSC and oscillograms of the fault current  $I$  when no HTSC are present in the sample. In this case, the depth of the current limiting was  $i_f / i_{lim} \gg 7$ .

The oscillograms of current and voltage with different weight additives of nano-dispersed  $\text{ZrO}_2$  powder, obtained at  $R_1 = 0$ , are shown in Figure 5b.

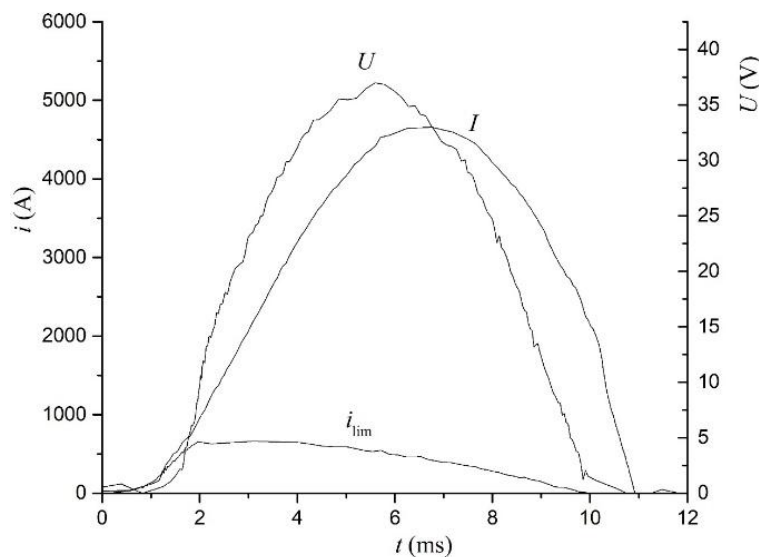


Figure 5a. Oscillograms of fault current  $I$ , limiting current  $i_{lim}$  and voltage  $U$  for a sample of HTSC without addition of nano-dispersed  $ZrO_2$  powder.

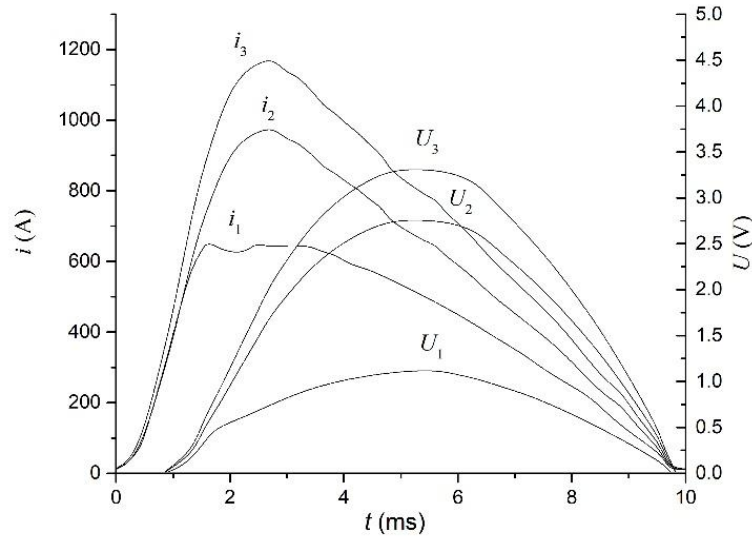


Figure 5b. Oscillograms of voltage and current for the sample of HTSC with different content of nano-dispersed powder  $ZrO_2$ : 1 – 4 wt.%, 2 – 8 wt.%, 3 – 12 wt. %.

When the content of the nano-dispersed  $ZrO_2$  powder increased, the character of changing the voltage and current on the sample coincided with the critical current calculated from the magnetization loops. Therewith, the delay in the moment of appearing the voltage on the HTSC element increased. A characteristic feature of the change in the current and the voltage over time is the presence of the moment at which a noticeable decrease in the rate of the current and the voltage rise occurred. This moment corresponds to the heating of the HTSC and the beginning of its transition to the normal state. The transition time of the HTSC from the superconducting to the normal state varied depending on the content of the nano-dispersed  $ZrO_2$  powder from 1 ms to 1.5 ms.

**Conclusion.** Thus, it was found that the addition of nanoscale  $ZrO_2$  particles leads to an increase in the critical current density at  $T = 77$  K for concentrations of 4-12 wt.%. Such an increase in the critical current is associated with  $ZrO_2$  nanoparticles that appear on the surface of superconducting granules. These granules become effective pinning centers for the Abrikosov vortex. As the temperature rises, effective pinning occurs on larger  $ZrO_2$  particles. The performed experiments demonstrated the effectiveness of the proposed approach to the problem of limiting and disconnecting a fault current in AC circuits.

**Acknowledgment.** The work was performed with a support of the grant of the Russian Science Foundation (project no. 16-19-10054)

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