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Direction Finding in Satellite Systems

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In article the method allowing to determine coordinates of a source a radio emission located on a terrestrial surface in satellite systems with use of the geostationary satellite is stated.

Keywords: determination of coordinates, radio emission source, satellite systems, difference of phases

Пеленгация в спутниковых системах

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В статье описан метод, позволяющий определить координаты источника радиоизлучения, расположенного на земной поверхности, в спутниковых системах с использованием геостационарного спутника.

Ключевые слова: определение координат, источник радиоизлучения, спутниковые системы, разность фаз.

Introduction

In satellite technologies the problem determination of coordinates a source a radio emission (SRE) which can settle down both on Earth surface, and on the aero-space carrier [1] is actual.

Method determination of location SRE

For measurement of coordinates the SRE (corners α and β in topocentric system of coordinates, Fig. 1), B_g located in a point the phase radio direction finder established onboard a communication

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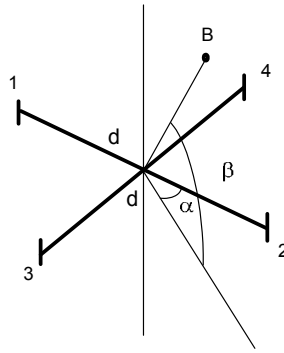


Fig. 1. Antenna arrays

artificial satellite (ASE), has to have two couples antennas 1-2 and 3-4 with mutually perpendicular bases. Shift of phases between E.D.S., induced in antennas 1-2 and 3-4, [2]:

$$\Delta\psi_{1-2} = \frac{2 \cdot \pi \cdot d}{\nu} \cdot \sin \alpha \cdot \cos \beta, \quad \Delta\psi_{3-4} = \frac{2 \cdot \pi \cdot d}{\nu} \cdot \cos \alpha \cdot \cos \beta \quad (1)$$

Where: d – base of antennas 1-2 and 3-4; ν – length of a wave an accepted signal.

Corners α and β from (1):

$$\alpha = \arctg \frac{\Delta\psi_{1-2}}{\Delta\psi_{3-4}}, \quad \beta = \arccos \frac{\nu}{2 \cdot \pi \cdot d} \cdot \sqrt{\Delta\psi_{1-2}^2 + \Delta\psi_{3-4}^2}. \quad (2)$$

Having placed an antenna arrays on a geostationary ASE it is possible to define the direction on SRE concerning an ASE [3 ... 6]. For determination of coordinates SRE it is necessary to calculate its coordinates in geocentric system of coordinates taking into account ellipticity of Earth

For calculation of required width and longitude of a source signal we will address to Fig. 2 [7]. Transition to the geocentric demands modification of expressions (2) therefore corners α and β pay off on formulas from topocentric system of coordinates:

$$\alpha = \arctg \frac{\Delta\psi_{3-4}}{\Delta\psi_{1-2}}, \quad \beta = \arcsin \frac{\nu}{2 \cdot \pi \cdot d} \cdot \sqrt{\Delta\psi_{1-2}^2 + \Delta\psi_{3-4}^2}. \quad (3)$$

Here $\alpha = 90 - \alpha_1$; $\beta = 90 - \beta_1$.

The point D_g lies in the plane of the equator and is the projection of a point B_g . The angle φ of the triangle $B_g O D_g$ is the breadth of the signal source. The longitude λ of the signal source is $\lambda = \lambda_{sp} + \lambda_g$, where λ_g – angle triangle $C_g O D_g$; λ_{sp} – longitude of the satellite. If the satellite is on the Greenwich Meridian, $\lambda_{sp}=0$. The point C_g on the line $R1$ is a projection of a point D_g on the meridional plane. Note that $R1=42253,135$ km [8].

To determine λ_g refer to the section of the Earth meridional plane (Fig. 3b). In the triangle $K_g O N_g$ angle α is calculated according to the formula

Segment $K_g N_g$ is perpendicular to the plane of the equator. Required in this triangle is the n -end. Fig. 3a shows the plane spheroid with minor radius n , at an angle α to the plane of the equator. Semi-minor axis n intersects the plane of a triangle $B_g A O$ at the same angle α to the plane of the equator. In

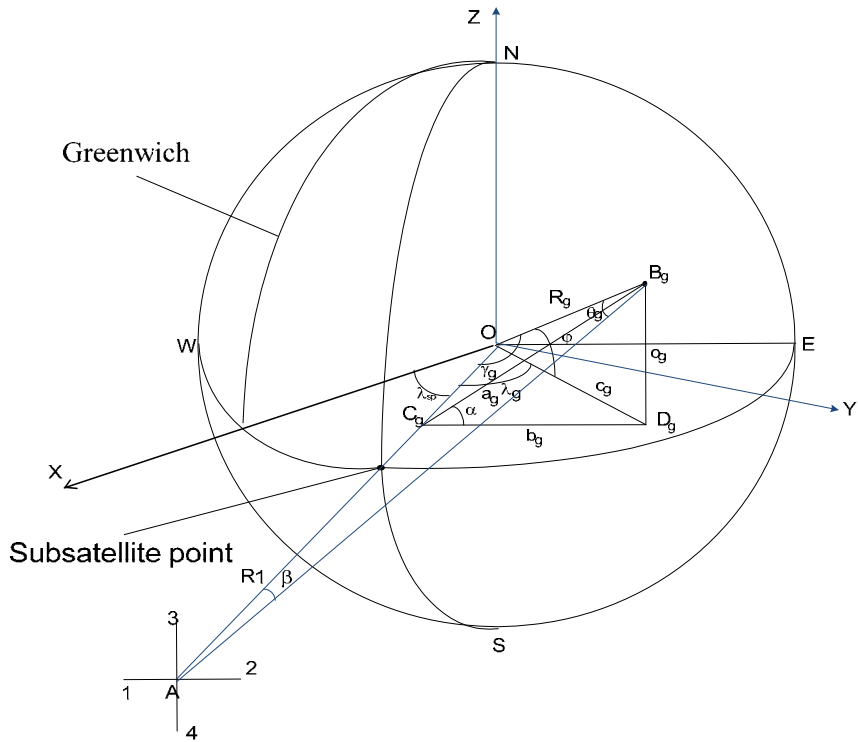


Fig. 2. Geometrical ratios

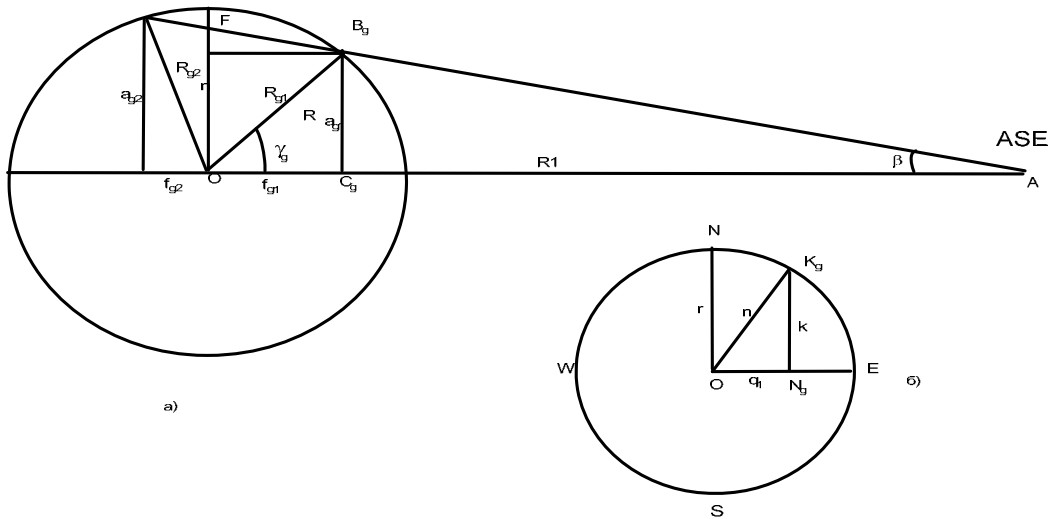


Fig. 3. Additional geometric constructions to calculate the coordinates of SRE with regard to the ellipticity of the Earth

the triangle B_gAO angle β is calculated according to the formula (3). The required Fig. 3a is a R_g party in the triangle B_gAO .

Calculation of latitude ϕ and longitude λ includes the following 7 stages.

1. Is the point of intersection (Fig. 3b) minor axis n and arc spheroid, the solution of systems of two equations

$$\left. \begin{aligned} k &= q \cdot \operatorname{tg} \alpha \\ k &= r \cdot \sqrt{1 - \frac{q^2}{R^2}} \end{aligned} \right\}. \quad (4)$$

where the first equation describes the minor axis, and the second is arc of a spheroid.

The solution (4) has two roots

$$q_1 = r \cdot R \cdot \sqrt{\frac{1}{\operatorname{tg}^2 \alpha \cdot R^2 + r^2}}, \quad q_2 = -r \cdot R \cdot \sqrt{\frac{1}{\operatorname{tg}^2 \alpha \cdot R^2 + r^2}} \quad (5)$$

Further used only positive root, since a negative value belongs to the opposite part of a spheroid.

Substituted q_1 in any of the equations (4), we obtain the value of K . The semiminor axis n of a right triangle $K_g O N_g$ is equal to:

$$n = \sqrt{k^2 + q_1^2}. \quad (6)$$

2. Is the point of intersection (Fig. 3a) direct R_1 , which is given by the equation $a_g = \operatorname{tg}(R_1 - f_g)$ and arc spheroid by solving the system of two equations:

$$\left. \begin{aligned} a_g &= \operatorname{tg}(R_1 - f_g) \\ a_g &= n \cdot \sqrt{1 - \frac{f_g^2}{R^2}} \end{aligned} \right\}. \quad (7)$$

Solution of the quadratic equation

$$\left(\operatorname{tg}^2 \beta + \frac{n^2}{R^2} \right) \cdot f_g^2 - 2 \cdot R_1 \cdot \operatorname{tg}^2 \beta \cdot f_g + (\operatorname{tg}^2 \beta \cdot R_1^2 - n^2) = 0, \quad (8)$$

are the two roots f_{g1} и f_{g2}

$$f_{g1} = \frac{2 \cdot R_1 \cdot \operatorname{tg}^2 \beta + \sqrt{D}}{2 \cdot (\operatorname{tg}^2 \beta + \frac{n^2}{R^2})}, \quad f_{g2} = \frac{2 \cdot R_1 \cdot \operatorname{tg}^2 \beta - \sqrt{D}}{2 \cdot (\operatorname{tg}^2 \beta + \frac{n^2}{R^2})}, \quad (9)$$

where $D = (2 \cdot R_1 \cdot \operatorname{tg}^2 \beta)^2 - 4 \cdot (\operatorname{tg}^2 \beta + \frac{n^2}{R^2}) \cdot (\operatorname{tg}^2 \beta \cdot R_1^2 - n^2)$.

From Fig. 3a and (9) follows that, in further calculations will need the root f_{g1} meaning equal side $O C_g$. Substituting f_{g1} into any equation of system (7), we obtain the value of the side a_{g1} , then from a right-angled triangle $B_g O C_g$, we find R_{g1} :

$$R_{g1} = \sqrt{a_{g1}^2 + f_{g1}^2}. \quad (10)$$

3. From right-angled triangle $B_g C_g D_g$ (Fig. 2) we find o_g :

$$o_g = a_{g1} \cdot \sin \alpha. \quad (11)$$

4. From right-angled triangle $B_g O D_g$ we find latitude φ of SRE:

$$\varphi = \arcsin \frac{o_g}{R_{g1}}. \quad (12)$$

5. From right-angled triangle $B_g O D_g$ we find c_g :

$$c_g = \sqrt{R_{g1}^2 - o_g^2}. \quad (13)$$

6. From right-angled triangle $B_g O C_g$, angle λ_g :

$$\lambda_g = \arccos \frac{f_{g1}}{c_g}. \quad (14)$$

7. Longitude λ of SRE:

$$\lambda = \lambda_{sp} + \lambda_g. \quad (15)$$

In geocentric system of coordinates (Fig. 2):

$$x = c_g \cos \lambda, y = c_g \sin \lambda, z = o_g. \quad (16)$$

Conclusion

Thus, the described technique relying on use onboard the spacecraft of an antenna arrays, allows to solve a problem determination of coordinates of the Source a radio emission.

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