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Quentin Galand – 0000-0001-5922-8585

Stéfan Van Vaerenbergh – 0000-0002-6614-0458

Werner Köhler –

Oleg Khlybov –

Tatyana Lyubimova –

Aliaksandr Mialdun – 0000-0002-7787-2865

Ilya Ryzhkov –

Valentina Shevtsova – 0000-0001-6109-5048

Thomas Triller – 0000-0002-7763-7865

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# Results of the DCMIX1 experiment on measurement of Soret coefficients in ternary mixtures of hydrocarbons under microgravity conditions on the ISS

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Quentin Galand,<sup>1,a)</sup> Stéfan Van Vaerenbergh,<sup>1</sup> Werner Köhler,<sup>2</sup> Oleg Khlybov,<sup>3</sup> Tatyana Lyubimova,<sup>3</sup> Aliaksandr Mialdun,<sup>1</sup> Ilya Ryzhkov,<sup>4,5</sup> Valentina Shevtsova,<sup>1</sup> and Thomas Triller<sup>2</sup>

## AFFILIATIONS

<sup>1</sup>MRC, Université libre de Bruxelles, Department of Chemical Physics, Avenue F. D. Roosevelt, CP165/32, B-1050 Brussels, Belgium

<sup>2</sup>Physikalisches Institut, Universität Bayreuth, 95440 Bayreuth, Germany

<sup>3</sup>Institute of Continuous Media Mechanics UB RAS, Koroleva, 1, 614013 Perm, Russia

<sup>4</sup>Institute of Computational Modelling SB RAS, 660036 Krasnoyarsk, Russia

<sup>5</sup>Siberian Federal University, Svobodny 79, 660041 Krasnoyarsk, Russia

<sup>a)</sup>E-mail: qgaland@ulb.ac.be. Tel.: (+32)26506576. Fax: (+32)26503126.

## ABSTRACT

The Soret coefficients of a set of ternary systems of 1,2,3,4-tetrahydronaphthalene (THN), isobutylbenzene (IBB), and n-dodecane ( $nC_{12}$ ) at 298.15 K were measured under microgravity condition aboard the International Space Station in the frame of the DCMIX1 experiment. The present work includes a comprehensive study of possible data processing sequences for the interpretation of interferometric Soret experiments in ternary systems. Several data processing methodologies are discussed. A significant concentration dependence of the Soret coefficients is observed. In the present study, we have obtained large and positive values for THN and negative ones for IBB in all investigated systems. A linear relation between the Soret coefficients of two components is derived for each system and allows validating experimentally the coefficients measured in other experiments.

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## I. INTRODUCTION

The study of thermodiffusion in multicomponent systems raises a great level of interest in the scientific community. Molecular diffusion and thermodiffusion play an important role in many natural<sup>1,2</sup> and industrial<sup>3</sup> processes and for the fundamental understanding of the behavior of liquid mixtures.<sup>4-6</sup> Thermodiffusion, or the Soret effect,<sup>7</sup> refers to a species transfer mechanism due to a local temperature gradient. The experimental techniques for the measurement of Soret coefficients in binary mixtures are well known and were presented in several reviews.<sup>8-11</sup> In recent years, a large amount of experimental work was devoted to the study of the Soret effect in multicomponent systems.<sup>12</sup>

In the present paper, we provide the Soret coefficients obtained from the measurements performed in ternary liquid systems aboard the International Space Station (ISS) during the DCMIX1 (Diffusion Coefficient Measurements in mIXtures) experiment. DCMIX1 is part of the DCMIX program that is endorsed by the European Space Agency and includes four experiments, studying several ternary liquid systems. During the DCMIX1 measurement campaign, a series of experimental runs were performed, studying ternary mixtures composed of 1,2,3,4-tetrahydronaphthalene (THN), isobutylbenzene (IBB), and n-dodecane ( $nC_{12}$ ) with different concentrations at 25 °C. The experimental conditions are such that species transport results from the combined effect of thermal gradient and molecular diffusion. In a ternary system, the diffusive flux  $J_i$  of component  $i$

53 can be written as<sup>13</sup>

$$54 \quad J_i = -\rho \sum_{j=1}^2 D_{ij} \nabla w_j - \rho D'_{T,i} \nabla T, \quad (1)$$

55 where  $\rho$  is the density of the liquid,  $D_{ij}$  are the molecular dif-  
56 fusion coefficients,  $w_i$  and  $D'_{T,i}$  are, respectively, the mass frac-  
57 tion and thermodiffusion coefficient of component  $i$ , and  $T$  is the  
58 temperature.

59 Significant data analysis and processing work is required in  
60 order to retrieve accurate values for the Soret coefficients. The raw  
61 data were simultaneously analyzed by several research teams and  
62 compared prior to publication. In the present paper, we detail the  
63 experimental setup and procedure, compare the different data pro-  
64 cessing methodologies, and report and discuss the obtained Soret  
65 coefficients.

## 66 II. EXPERIMENTAL

67 In this section, we discuss several aspects of the experiments.  
68 First, we explain the principle of the experimental technique in  
69 Sec. II A. The choice of the studied systems, the experimental setup,  
70 and the experimental procedures are described in Sec. II B.

### 71 A. DCMIX experiment

72 The principle of the DCMIX experiment was proposed in  
73 Ref. 14 for the experimental determination of the diffusion coeffi-  
74 cients of liquid mixtures. The concentration gradient used to observe  
75 molecular diffusion is created through the Soret effect by plac-  
76 ing the liquid in a nonuniform temperature field. This idea was  
77 already used in a number of previous studies, such as the laser beam  
78 deflection technique by Kolodner in 1987,<sup>15</sup> but here the chemi-  
79 cal composition field is observed by the means of an interfero-  
80 metric technique. Modern interferometric techniques allow obtain-  
81 ing a map of the chemical composition in liquid systems with a  
82 high spatial and temporal resolution. The Selectable Optical Diag-  
83 nostic Instrument (SODI) allows obtaining in one single experi-  
84 ment both the Soret and the diffusion coefficients. In this paper,  
85 the study is limited to the determination of the Soret coefficients  
86 only.

87 The experiment starts with a homogeneous system at constant  
88 temperature; at the beginning of the “Soret step” of a run, a tem-  
89 perature gradient is created in the liquid by placing the bottom and  
90 top walls of the liquid volume at two different temperatures. The  
91 temperature gradient is kept constant, and thermodiffusion induces  
92 the migration of the components. Once the system has reached a  
93 steady state, in a closed cell, with no convection and no chemical  
94 reaction, the diffusion fluxes vanish and the composition gradient  
95 along the cell is proportional to the temperature gradient. From Eq. (1),  
96 this can be written as

$$96 \quad \nabla w_i = -S'_{T,i} \nabla T, \quad (2)$$

97 where we introduced the modified Soret coefficients  $S'_{T,i}$ . 99% of  
98 the separation is obtained after about five times the characteris-  
99 tic diffusion time. In ternary systems, characteristic diffusion time  
100  $\tau = L^2/(\pi^2 D_s)$  can be computed using the cell height  $L$  and the  
101 smaller eigenvalue  $D_s$  of the diffusion matrix.<sup>16</sup> This corresponds  
102 to the end of the Soret step of the runs in on-board operations.

103 The so-obtained concentration differences  $\Delta w_i$  of the components  
104 across the cell provide the Soret coefficients by the relation

$$105 \quad \Delta w_i = -S'_{T,i} \Delta T, \quad (3)$$

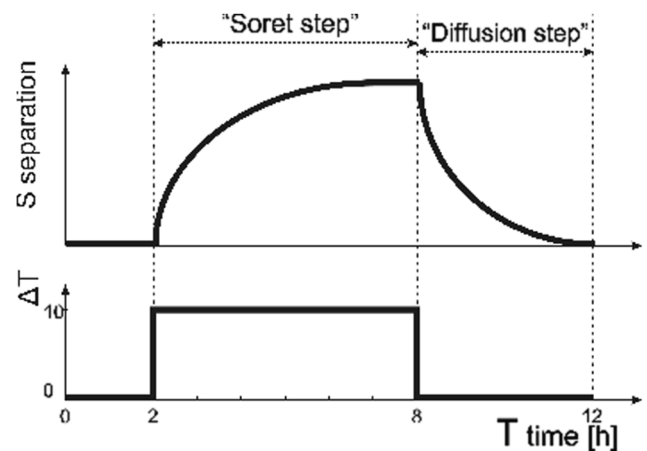
106 where the differences  $\Delta$  are from the top wall with respect to the  
107 bottom wall of the cell. After the Soret step, the temperature gradient  
108 is removed; the “Diffusion step” then develops and Eq. (1) applies  
109 with a vanishing temperature gradient,

$$110 \quad J_i = -\rho \sum_{j=1}^2 D_{ij} \nabla w_j. \quad (4)$$

111 The typical timeline of an experimental run is shown schemat-  
112 ically in Fig. 1.

### 113 B. Experimental

114 The primary objective of the DCMIX1 experiment is to obtain  
115 accurate and reliable experimental data about the diffusive proper-  
116 ties of multicomponent systems, in a convection free environment.  
117 The project originated from the collaboration between several acade-  
118 mic research centers with partners from the oil industry dur-  
119 ing which binary, ternary, and quaternary Soret coefficients were  
120 obtained in microgravity conditions in the SCCO experiment.<sup>17–19</sup>  
121 Three chemical species were selected to represent three major fami-  
122 lies of compounds found in crude oils: THN, IBB, and nC<sub>12</sub>, respec-  
123 tively, for the families of naphthenic, aromatic, and aliphatic com-  
124 pounds. The selected systems involve three components and are  
125 away from the dilution limits. Nondiluted ternary systems carry  
126 the main aspects of multicomponent systems, and chemo-diffusive  
127 couplings specific to multicomponent systems appear as soon as  
128 more than two nondiluted components are diffusing. The concen-  
129 trations of the systems investigated in DCMIX1 are summarized in  
130 Table I.



131 FIG. 1. Principle of an interferometric Soret diffusion experiment. Prior to the  
132 experiment, during the thermalization phase, the entire cell is kept at constant  
133 temperature. During the “Soret step,” a temperature gradient is applied to the liq-  
134 uid and the Soret effect induces a gradient of the chemical components in the  
135 system. During the “Diffusion step,” the temperature gradient is removed and the  
136 diffusion coefficients are quantified by observing the relaxation of the liquid induced  
137 by molecular diffusion.

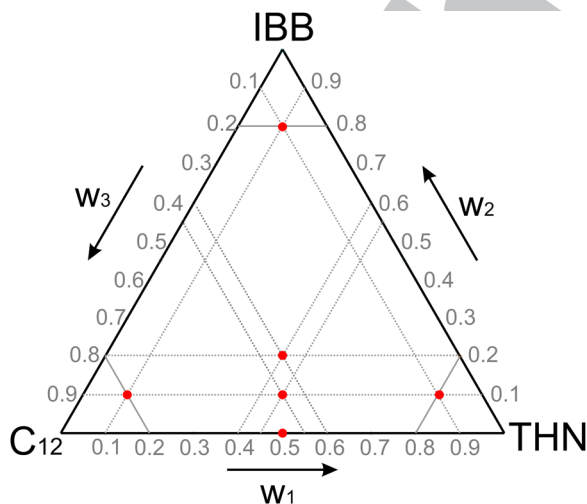
138 **TABLE I.** Concentrations of the systems investigated in the DCMIX1 experiment.

Cell	Component mass fraction (%)			Experimental runs processed in this study
	THN	IBB	nC <sub>12</sub>	
0	50	...	50	NA
1	10	10	80	16, 21
2	10	80	10	2 <sup>E</sup> , 07, 17, 22, 27
3	80	10	10	See Ref. 12
4	45	10	45	4 <sup>E</sup> , 19, 24
5	40	20	40	5 <sup>E</sup> , 15, 20, 25

150 In Fig. 2, the mixtures investigated in DCMIX1 are shown with  
151 red points. Five primary cells, cells 1–5, were filled with ternary mix-  
152 tures, and one companion cell, cell 0, was used to study a binary  
153 system with equal mass fractions of THN and nC<sub>12</sub>. The composi-  
154 tions are such that points are aligned in the ternary concentration  
155 diagram, with the aim of investigating mixing rules.<sup>17,20–23</sup>

156 The diffusion and Soret coefficients of the correspond-  
157 ing binary systems have been measured by several experimen-  
158 tal techniques in the frame of the Fontainebleau benchmark,<sup>24,25</sup>  
159 and the ternary diffusion coefficients were recently measured on  
160 ground.<sup>12,16,26,27</sup> For each system investigated during the DCMIX1  
161 campaign aboard the ISS, several experimental runs were performed.  
162 For cell 1, liquid leaked out of the cell during the measurement  
163 campaign. A bubble appeared in the cell, and only two experimental runs  
164 were completed.

165 For each cell, two different durations of the runs were used.  
166 In addition to the “standard runs,” “extended runs,” denoted with  
167 superscript *E* in tables Table I, have been proposed in the event that



168 **FIG. 2.** Concentrations of the systems investigated in DCMIX1. The concentrations  
169 of the systems investigated under microgravity conditions in DCMIX1 are shown  
170 by red dots in a ternary diagram. Systems characterized by aligned points in the  
171 diagram were selected for the investigation of mixing rules.

172 the diffusion coefficients of one investigated system are significantly  
173 lower than foreseen.

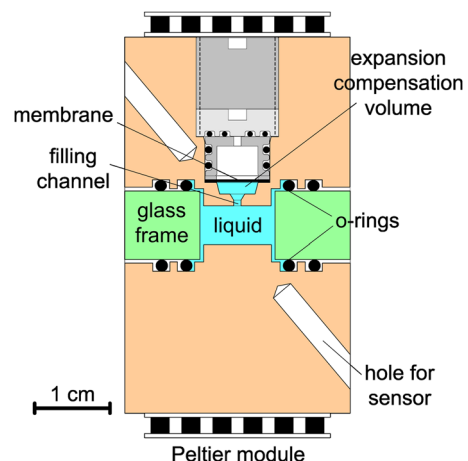
174 Each run starts with a thermalization phase during which the  
175 temperature of the cell is stabilized to 25 °C. The top and bottom  
176 cell walls are then brought to 20 and 30 °C, respectively. A stationary  
177 temperature gradient quickly establishes in the liquid, and the ther-  
178 modiffusion process is monitored during a given time. The tempera-  
179 ture gradient is then removed, and isothermal diffusion is observed.  
180 The duration of the “Soret step” was selected so that the Soret sep-  
181 aration attains the steady state. The duration of the “diffusion step”  
182 was chosen to cover several characteristic molecular diffusion times.

183 For some runs, data are acquired simultaneously for the com-  
184 panion cell and for a primary cell. The measurements in the com-  
185 panion cell are carried out in order to study the possible influence of  
186 the residual gravity on the experiments, a topic of interest for micro-  
187 gravity assessment,<sup>28–31,57</sup> and to cross-check with ground based  
188 measurements.

189 The liquid is placed in a parallelepipedic cell, as shown in  
190 Fig. 3. The four lateral sides of the cell are transparent, allowing  
191 optical probing. The temperatures of the upper and lower metallic  
192 walls of the cell are controlled precisely and independently by  
193 Peltier modules. During the DCMIX1 measurement campaign, the  
194 six systems presented in Table I are arranged in a cell array and stud-  
195 ied sequentially.<sup>32</sup> Details regarding the cell design can be found in  
196 Ref. 26.

197 The chemical composition within the binary system of the  
198 companion cell is visualized with a standard Mach-Zehnder type  
199 interferometer. A movable two-wavelength interferometer, which  
200 can be moved to the selected cell, probes the primary cells.<sup>33</sup>  
201 The wavelengths of the laser diodes used are  $\lambda_1 = 670$  nm and  
202  $\lambda_2 = 935$  nm.

203 The components of the experimental setup were assembled  
204 inside the US Destiny module where ISS residual gravity is lowest.  
205 A set of parameters monitoring the functioning of the experiment  
206 are both simultaneously displayed in real time on ground and stored



207 **FIG. 3.** Schematic of a DCMIX experimental cell. The liquid volume is sealed by  
208 O-rings. Two Peltier elements are used to control the temperatures of copper parts.  
209 Temperature sensors probe the temperatures of the copper parts.

210 on flash disks. The data were distributed to the science team by the  
211 MARS center.<sup>34</sup>

### 212 III. DATA PROCESSING

213 The data obtained from the experiment are a set of digitized  
214 interferograms. The data processing methodology implemented to  
215 obtain the Soret coefficients from the experimental data consists of  
216 a sequence of five main steps. As discussed in Ref. 35, for each step,  
217 several possibilities can be envisaged; this results in a wide variety  
218 of data processing approaches, as shown diagrammatically in Fig. 4.  
219 During the course of previous benchmarking for DCMIX1,<sup>12</sup> several  
220 teams have processed the same set of experimental data by differ-  
221 ent processing schemes. The mass transfer coefficients, obtained  
222 by different procedures, have revealed large dispersion. To address  
223 this problem, in the present study, we investigate 7 data processing  
224 schemes, referred to as DP 1–7 in Table II, and we compare in detail  
225 the transport coefficients obtained.

226 The different possible implementations of the 5 steps of Fig. 4  
227 are discussed in the following.

228 The capital letters A to E refer to the major successive steps of  
229 the data processing sequence. The possible implementations of each  
230 step are indicated by numbered panels.

#### 231 A. Input experimental data

232 The first step of the data processing scheme is the selection of  
233 the experimental data used for the estimation of the transport coef-  
234 ficients. In Table II, data processing schemes 1–4 analyze the data  
235 collected during the *Soret phase* of an experimental run, while data  
236 processing schemes 5–7 use the data corresponding to the *diffusion*  
237 *phase* of the runs.

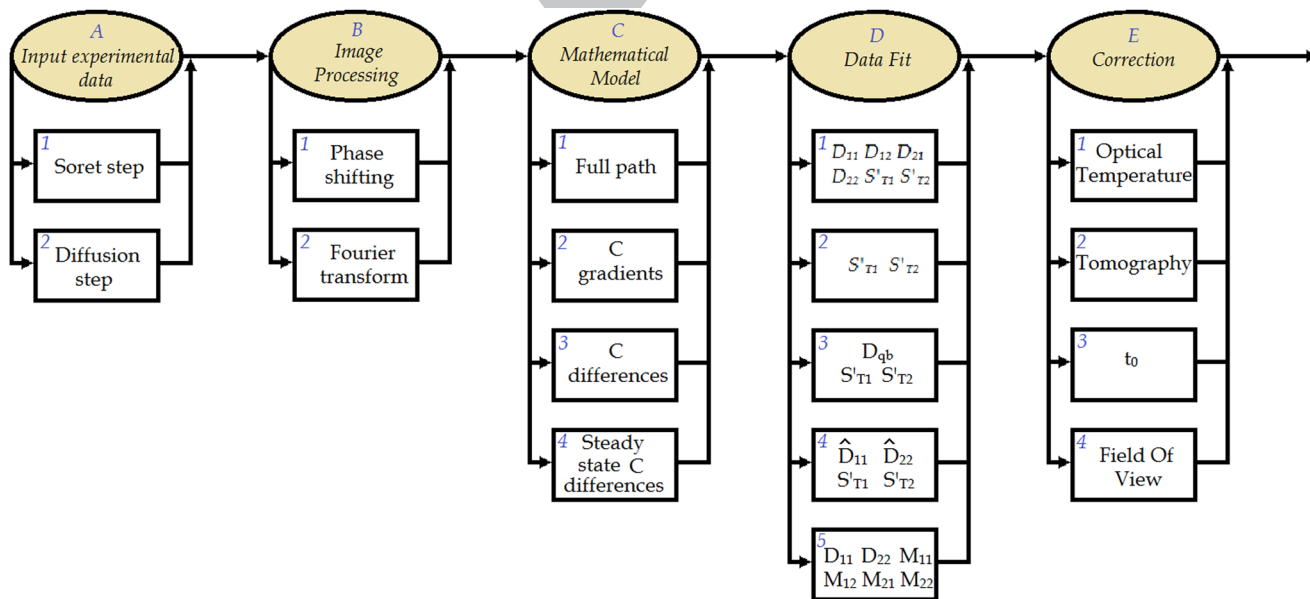
240 TABLE II. Data processing sequences used in the present study.

DP	Processing sequence	Authors
1	A1 B1 C1 D3 E3+4	AM, VS (ULB)
2	A1 B1 C1 D3 E2+3	AM, VS (ULB)
3	A1 B1 C3 D3 E4	TT, WK (UB)
4	A1 B2 C1 D4 E3+4	OK, IR, TL (RAS)
5	A2 B2 C1 D4 E3+4	OK, IR, TL (RAS)
6	A2 B1 C3 D2 E4	QG, SVV (ULB)
7	A2 B1 C1 D1 E4	QG, SVV (ULB)

250 In optical probing, the spatial concentration variation in the liq-  
251 uid is evaluated by measuring changes in the refractive index. During  
252 the Soret step of the experimental runs, the refractive index  $n$  of  
253 the ternary system varies with its temperature and with its chemical  
254 composition,

$$\Delta n_i = \left. \frac{\partial n_i}{\partial T} \right|_{w_1, w_2} \Delta T + \left. \frac{\partial n_i}{\partial w_1} \right|_{w_2, T} \Delta w_1 + \left. \frac{\partial n_i}{\partial w_2} \right|_{w_1, T} \Delta w_2, \quad (5)$$

256 where the symbol  $\Delta$  here denotes the changes of quantities with  
257 respect to their equilibrium values. The thermal and molecular dif-  
258 fusivities differ by about two orders of magnitude, and it is easy to  
259 separate the two last terms on the right hand side (RHS) of Eq. (5)  
260 from the thermal signal contribution. The thermal field is obtained  
261 from the early images of the *Soret step* of the runs, while the images  
262 recorded later are used to obtain the concentration changes  $\Delta w_1$   
263 and  $\Delta w_2$ . During the diffusion step of the experiments, the liquid  
264 is isothermal and the first term on the RHS of Eq. (5) vanishes. The  
265 fringe density significantly increases when the temperature gradient



238 FIG. 4. Simplified diagram of possible schemes for processing interferometric Soret-diffusion experimental data. The top panels A to E indicate the major successive steps.  
239 The possible implementations of each step are indicated by numbered panels.



is imposed across the cell, as easily observed from two experimental images shown in Fig. 5.

## B. Image processing

By design, the interpretation of interferometric experimental data requires the use of a 5 step image processing method. Before the image processing procedure, the images are cropped and rotated to exclude the regions outside the sample volume and to align the plates of the cell horizontally. The first step, the phase calculation, is the determination, directly from the interferograms, of a wrapped phase change  $\Psi$ . In the second step, a reference image is subtracted from every image since the individual phase values are meaningful only when compared to a reference state.  $\Delta\Psi$  is wrapped into the interval  $[-\pi, \pi]$ . The third step, phase unwrapping, allows obtaining the phase change  $\Delta\varphi$  of the light of wavelength  $\lambda$  traversing the sample along the geometrical path  $e$  that results from a refractive index change  $\Delta n$ ,

$$\Delta\varphi = \frac{2\pi e}{\lambda} \Delta n. \quad (6)$$

Finally, the unwrapped phase is converted into the refractive index using Eq. (6).

### 1. Phase calculation

The image acquisition technique used is a phase shifting interferometry.<sup>36,37</sup> It consists in acquiring several fringe images that are phase shifted by an integer fraction of  $2\pi$  of the object and calculating the resulting phase signal with a phase shifting algorithm. In SODI, phase shifts are obtained by stepping the laser diode currents. For DCMIX1, the selected technique is based on the acquisition of a set of five fringe images with a phase shift of  $\pi/2$ . The acquisition of five images is achieved within less than a second, a time where the refractive index field can be considered constant. This assumption is perfectly reasonable since the characteristic time of the experiments is of the order of several hours. In the data processing schemes DP 1 and 2 of Table II, phase images were computed using the Hariharan algorithm.<sup>38</sup> In DP3, a modified<sup>39</sup> version of the Hariharan equation was implemented.<sup>40</sup> In DP 4 and 5, the widely known Fourier filtering method<sup>41,42</sup> was applied. This method allows reconstructing the optical phase from a single interference image. A detailed description of the method is provided in Refs. 33 and 43. As discussed in Ref. 38, for many DCMIX images, significant phase shift errors were observed, resulting in strong disturbances of the phase signal when standard stepping algorithms are straightforwardly applied. In

DP 6 and 7, to address this problem, the phase signals were recovered with iterative algorithms.<sup>44</sup> All the above-mentioned methods differ substantially in their basic principles; therefore, one can expect some differences between the obtained signals. Note that even within the same methodology, difference in results obtained by different researchers may arise due to the implementation of the algorithms.

### 2. Reference subtraction

Interferometry, by principle, is a differential measuring technique: the measured quantity is the variation of the refractive index field with respect to a reference, commonly referred to as the “reference image.” When processing the images acquired during the Soret phase of the runs, the reference image corresponds to the beginning of the Soret phase, right after the establishment of the temperature gradient in the liquid, so that the reference subtraction allows separating the thermal and compositional parts of the experimental signals of Eq. (5). On the other hand, when performing the processing of the images of the diffusion phase of the runs, the reference image is acquired at the end of the thermalization phase of the runs, prior to the Soret phase.

### 3. Phase unwrapping

Phase unwrapping is a well-known problem in interferometry, and many different algorithms have been proposed to remove the phase ambiguity.<sup>45</sup> In DP1, DP2, and DP3, a modified<sup>40</sup> version of the Itoh algorithm<sup>46</sup> was implemented; in DP 4 and 5, the wrapped phase images are of sufficient quality, the phase exhibit a strict horizontal alignment, and a one-dimensional sequential phase unwrapper was employed;<sup>33</sup> in DP6 and 7, the Costantini<sup>47</sup> algorithm was used.<sup>48</sup>

### 4. Contrast factors

These image processing operations are performed independently for the two sets of images acquired for the two wavelengths of the two-color interferometer and allow obtaining two series of refractive index maps  $\Delta n_i(x, y, t)$ . The concentration fields are then obtained with the following equation:

$$\begin{pmatrix} \Delta w_1 \\ \Delta w_2 \end{pmatrix} = \begin{pmatrix} n_{1,1|2} & n_{1,2|1} \\ n_{2,1|2} & n_{2,2|1} \end{pmatrix}^{-1} \begin{pmatrix} \Delta n_1 \\ \Delta n_2 \end{pmatrix}, \quad (7)$$

where we introduced the optical contrast factors  $n_{i,j|k}$ , defined as

$$n_{i,j|k} = \frac{\partial n_i}{\partial w_j} \Big|_{T,P,w_k,k \neq j}. \quad (8)$$



FIG. 5. Comparison of typical interference patterns. Left: pattern recorded during the Soret phase of an experimental run. Right: pattern recorded during the diffusion phase.

349 **TABLE III.** Contrast factors for the 5 ternary systems studied in the DCMIX1 exper-  
350 iment at  $T = 25^\circ\text{C}$ . Component 1 is *THN*, component 2 is *IBB*, and component 3  
351 is nC12. Contrast factors are defined in Eq. (8). Those values were computed from  
352 Ref. 49.

Cell	$w_1$	$w_2$	$w_3$	$n_{1,1} _2$	$n_{1,2} _1$	$n_{2,1} _2$	$n_{2,2} _1$	$K$
1	10	10	80	0.0960	0.0547	0.0926	0.0521	342
2	10	80	10	0.1248	0.0758	0.1198	0.0714	254
3	80	10	10	0.1427	0.0887	0.1374	0.0838	241
4	45	10	45	0.1149	0.0686	0.1107	0.0655	495
5	40	20	40	0.1164	0.0696	0.1120	0.0667	1092

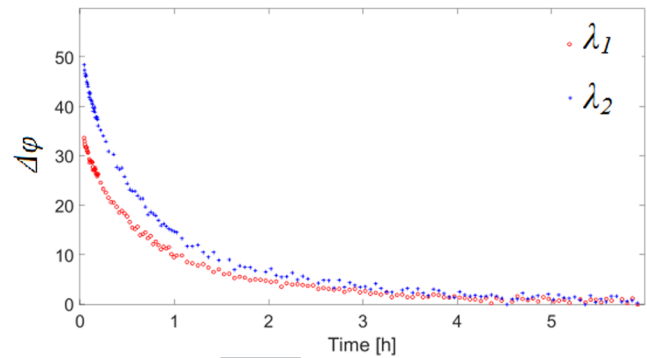
360 The contrast factors are experimentally measured in ground exper-  
361 iments. The computed values of the Soret coefficients strongly  
362 depend on the values of the contrast factors used for the calculations.  
363 In the present study, all teams used identical contrast factors, com-  
364 puted using the methodology and the experimental data reported in  
365 Ref. 49 and summarized in Table III.

366 An algorithm for identification of the transport coefficients  
367 requires the inversion of the matrix of optical contrast that can be  
368 ill conditioned.<sup>49</sup> The conditioning of a matrix is characterized by a  
369 condition number  $K$ .<sup>35</sup> The smaller the condition number, the lower  
370 the error amplification when computing the concentration of the  
371 components from the interferograms.

### 372 C. Data fitting

373 Identification of the mass transport coefficients is performed  
374 by fitting the analytical solution of Eq. (1) to the experimental data  
375 extracted from the processed images. The concentration distribu-  
376 tion can be written in different ways. The most widely used ana-  
377 lytical solutions are the full path solution<sup>26,35,43,51</sup> that includes all  
378 available data points, both in time and in space; the gradient solu-  
379 tion,<sup>33,35,52</sup> similar to the optical beam deflection (OBD) approach,<sup>53</sup>  
380 which describes the gradient of concentration at midheight of the  
381 cell; and the concentration difference solution,<sup>32,54</sup> which describes  
382 the temporal evolution of the difference of concentration between  
383 the top and the bottom of the cell. Each of the above provides both  
384 Soret and diffusion coefficients, but the amount of data involved in  
385 the identification of the mass transport coefficients is essentially dif-  
386 ferent and the use of the different approaches can lead to slightly  
387 different results. Finally, one can simply analyze the concentration  
388 gradient at steady state by processing the image obtained at the end  
389 of the Soret phase of the run (or alternatively at the beginning of  
390 the diffusion phase, as proposed in Ref. 48). This method allows retriev-  
391 ing the Soret coefficients directly with Eq. (2) and does not require  
392 identifying the diffusion coefficients. As can be seen from Fig. 6,  
393 the two phase signals obtained at different wavelengths are clearly  
394 separated from each other.

395 In general, the mathematical solution of a Soret diffusion exper-  
396 iment in ternary mixture comprises six unknowns, four diffusion  
397 coefficients  $D_{11}$ ,  $D_{12}$ ,  $D_{21}$ , and  $D_{22}$ , and two Soret coefficients  $S'_{T,1}$   
398 and  $S'_{T,2}$ . To obtain reliable fitting results, different strategies were  
399 tested in this study. In the first, as done in DP 7, the six unknowns  
400 are fitted directly. This technique, however, provides diffusion coef-  
401 ficients that are very sensitive to noise. Using specific combinations  
402 of unknown quantities in the analytical solutions, the problem can



403 **FIG. 6.** Typical phase signals obtained after image processing of the data of a  
404 DCMIX1 experimental run. The two optical signals, corresponding to the two wave-  
405 lengths of the two-color interferometer,  $\lambda_1 = 670\text{ nm}$ ,  $\lambda_2 = 935\text{ nm}$ , are of similar  
406 shape but different amplitude.

407 be converted to four parameters<sup>33</sup> (two Soret coefficients and two  
408 diffusion eigenvalues,  $\widehat{D}_1$  and  $\widehat{D}_2$ ). The mathematical details of  
409 different models are available elsewhere.<sup>35</sup> This methodology was  
410 applied in DP2 and DP3. Moreover, assuming that the two diffusion  
411 eigenvalues are equal,

$$412 \widehat{D}_1 = \widehat{D}_2 = D_{qb}, \quad (9)$$

413 meaning that ternary diffusion can be modeled as quasibinary diffu-  
414 sion, the problem is then simplified to a three-parameter fit.<sup>26</sup> This  
415 methodology was used in DP1 and DP2. In DP3 to DP5, the mathe-  
416 matical modeling requires defining an amplitude matrix  $M$ .<sup>27,52</sup> The  
417 fitting identifies 6 unknowns, the four elements of  $M$  and the two  
418 diffusion eigenvalues. Alternatively, in the steady state concentra-  
419 tion gradients method, used in DP6, only the two Soret coefficients  
420 are fitted.<sup>48</sup>

421 We want to emphasize that for the present work, the shapes  
422 of the transients and, hence, the diffusion eigenvalues, were not  
423 analyzed in full detail since they are irrelevant for the asymptotic  
424 amplitudes that determine the Soret coefficients. This becomes most  
425 apparent in the quasibinary approximation of Eq. (9), where the  
426 two eigenvalues are even set equal. The diffusion eigenvalues of the  
427 systems were measured elsewhere, by the Taylor Dispersion Tech-  
428 nique (TDT),<sup>16</sup> by the Optical Beam Deflection (OBD),<sup>52</sup> and by  
429 the Sliding Symmetric Tubes (SST).<sup>55</sup> Additional experimental data  
430 obtained by the SST<sup>56</sup> and by the open ended capillary method<sup>48</sup>  
431 were also reported for cell 3 in the frame of a benchmark.<sup>12</sup> Those  
432 data are summarized in Table IV.

### 433 D. Corrections

434 Due to the DCMIX cell design, the temperature field in the  
435 liquid is not perfectly linear. As a consequence, see Eq. (1), the con-  
436 centration distribution, and therefore the measured refractive index  
437 fields, is also not linear. However, the working equations describing  
438 the problem apply linear concentration profiles. As a consequence,  
439 optical integration of the deformed refractive index fields leads to  
440 underestimated values of the Soret separation. Different suggestions  
441 for the correction of the data were proposed. In Ref. 32, the authors  
442 use a so-called “optical temperature” (see Sec. IV A) in Eq. (3) to



**TABLE IV.** Diffusion eigenvalues and mean eigenvalue  $\bar{D}$  for the DCMIX1 systems. Those values were obtained by the Taylor Dispersion Technique (TDT) in Ref. 16, by the optical beam deflection in Ref. 52, by the Sliding Symmetric Tubes (SST) in Refs. 55 and 56, and by the open ended Capillary in Ref. 48.

C	Reference	$\hat{D}_1$ ( $10^{-10}$ m <sup>2</sup> s <sup>-1</sup> )	$\hat{D}_2$ ( $10^{-10}$ m <sup>2</sup> s <sup>-1</sup> )	$\bar{D}$ ( $10^{-10}$ m <sup>2</sup> s <sup>-1</sup> )
1	TDT <sup>16</sup>	11.9	8.8	10.35
	OBD <sup>52</sup>			6.02
	SST <sup>55</sup>	11	9	10
2	TDT <sup>16</sup>	10.9	9	9.95
	OBD <sup>52</sup>			9.82
	SST <sup>55</sup>	12	9	10.5
3	Benchmark <sup>12</sup>	6.61	5.48	6.04
	TDT <sup>16</sup>	7.4	5.3	6.35
	OBD <sup>52</sup>			9.29
	OEC <sup>48</sup>	6.60	5.50	6.05
	SST <sup>55</sup>	8.08	5.43	6.75
4	TDT <sup>16</sup>	8.5	6.2	7.35
	OBD <sup>52</sup>			6.65
	SST <sup>55</sup>	7	7	7
5	TDT <sup>16</sup>	8.9	6.5	7.7
	OBD <sup>52</sup>			7.03
	SST <sup>55</sup>	7	4	5.5

compute the Soret coefficients. In the present study, all the Soret coefficients were computed with a temperature difference of 10 °C, as measured by the temperature sensors. In Refs. 26, 35, 57, and 58, the authors recommend performing a tomography reconstruction of the concentration profiles in the center of the cell to account for the curvature of the temperature field. This approach is used in DP2 in our study.

At short times, both in the Soret and the diffusion phase of the runs, the hypothesis of the temporal separation of the thermal and compositional transients is not strictly valid.<sup>30</sup> During the temperature transient, diffusive concentration changes do happen close to the top and bottom walls of the cell,<sup>59</sup> but are not observed in the interferograms, due to the reference image subtraction. In DP1, DP2, DP4, and DP5, this effect is taken into account by introducing an additional fitting variable, an initial time  $t_0$ , as discussed in Refs. 26, 33, and 43.

The temperature field in the cell is more linear in the central part, and more curved in the external regions of the cell, approaching the upper and lower heating elements or the Quartz walls. DP 4, DP5, DP6, and DP7 only take into account a limited central region of the field of view of the interferograms.

## IV. RESULTS AND DISCUSSION

### A. Thermal analysis

The thermal regulation timeline of the cells includes several steps. We present in the following figures the typical evolution of

the temperatures  $T_1$  and  $T_2$  in the top and bottom part of each experimental cell. For all the runs for cells 0–4, the performance of the temperature regulation was very similar. A typical plot of the temperatures  $T_1$  and  $T_2$  for those runs is showed in Fig. 7.

In Fig. 7, the speed of the regulation during the buildup and the removal of the temperature gradient are illustrated by temporal zooms. For all the runs, 90% of the temperature gradient is established or removed within a little less than 1 min and more than 99% is stabilized within 2 min. The third zoom shows that the temperature regulation is stable and precise: during the *Soret step*, the maximum deviation between the measured and set point temperatures is 0.02 °C; during the *diffusion step*, it is 0.05 °C. Similar temperature profiles were observed for all runs for cells 0–4. For all runs on cell 5 however, notable deviations from the nominal temperatures were observed throughout the experiments, as depicted in Fig. 8. The cause of the occasional malfunction of the temperature regulation for this cell could not be revealed.

For those runs, numerous temperature spikes were detected, during which the difference between the set-point and measured temperatures was of the order of 0.2–0.4 °C.

As mentioned earlier, the characteristic heat and mass diffusion times differ by about two orders of magnitude. The analysis of the interferometric data at the beginning of the *Soret step* allows obtaining information about the temperature field across the cell. We report here the data obtained for the binary system, referred to as cell 0 in Table I. Both temperatures were stabilized at 25 °C before acquiring a reference image.  $T_1$  was then raised to 30.00 °C,

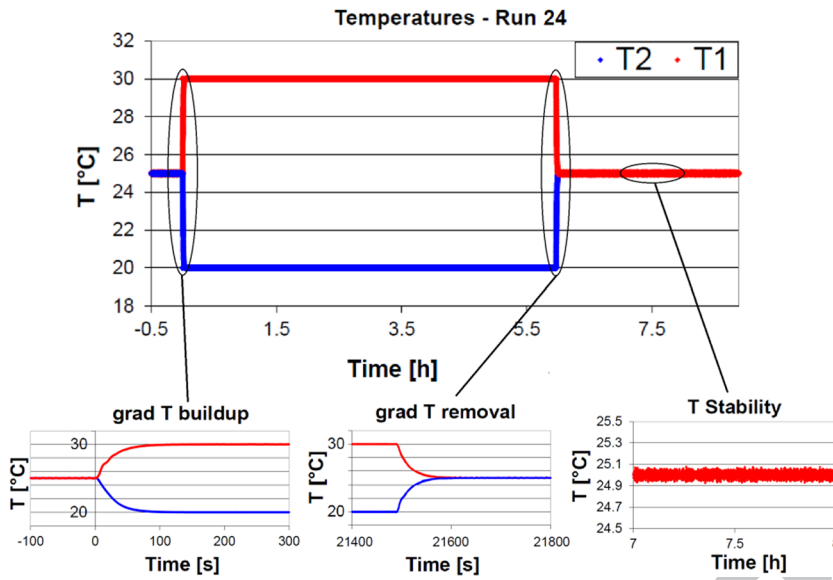


FIG. 7. Typical temperature cycle performed in a DCMIX1 run for cells 0–4. In the bottom of the figure, several zooms are shown to illustrate the performances of the temperature regulations.

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515 while  $T_2$  was cooled down to 20.00 °C. 2 min later, a second interferometric image was acquired. This corresponds to more than  
516 5 times the characteristic heat diffusion time for the investigated  
517 liquids. The corresponding phase images were calculated and processed  
518 as described in Fig. 9. The observed phase change is shown in  
519 Fig. 10.

520 A map of the refractive index change was calculated with  
521 Eq. (10). Interferometry measures the average refractive index

change across the liquid sample (here, average means integrated  
531 along the optical axis of the interferometer). It is then possible to  
532 determine a 2D map of the average temperature in the liquid, the  
533 “optical temperature”  $T_{opt}$ ,  
534

$$T_{opt} = \frac{\Delta n_1}{n_{1,T}}, \quad (10)$$

535

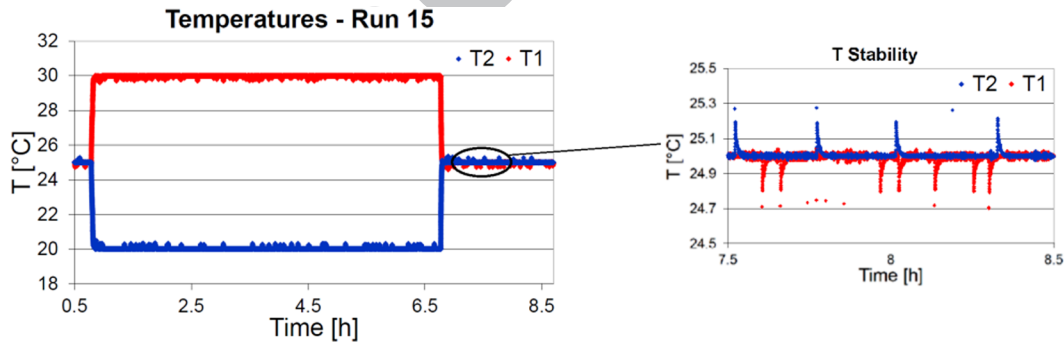


FIG. 8. Typical temperature cycle performed in a DCMIX1 run for cell 5. These measurements show that temperature control did not function nominally for cell 5. Notable deviations from the nominal temperatures were observed. The cause of the malfunction could not be revealed.

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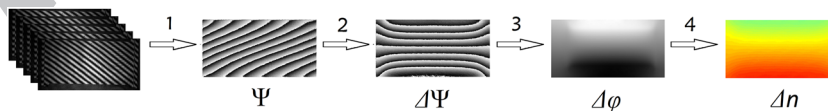
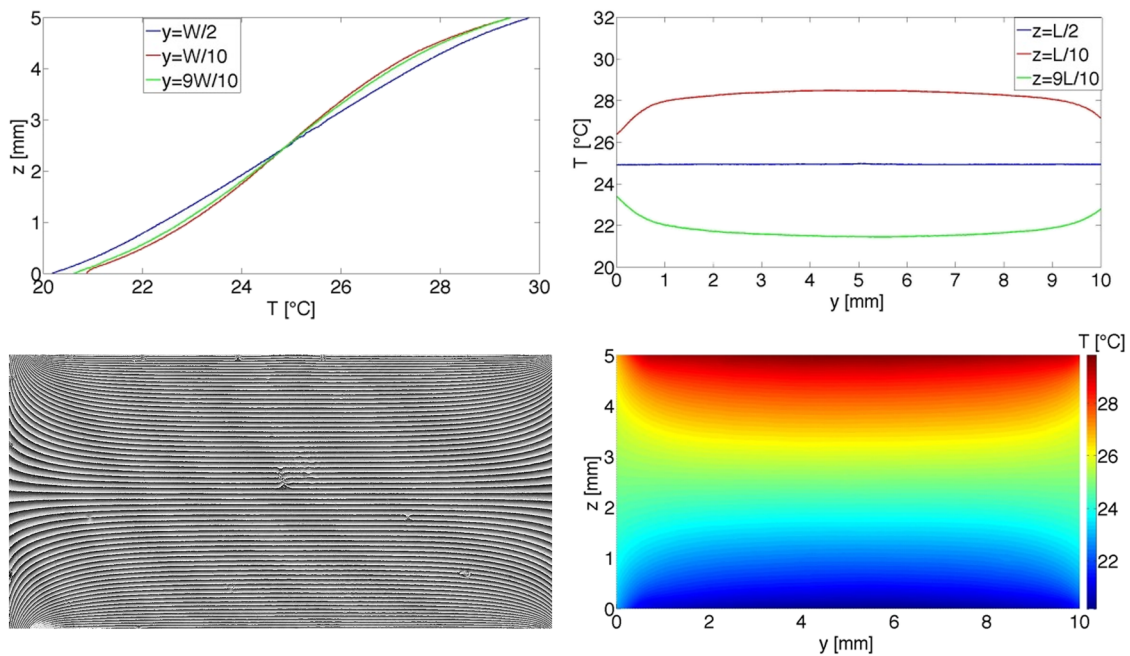


FIG. 9. Image processing steps for the translation of interferometric experimental of a Soret diffusion experiment. Step 1 is phase calculation, step 2 is reference image subtraction, step 3 is phase unwrapping, and step 4 is computation of refractive from the unwrapped phase.

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**FIG. 10.** Temperature field in cell 0. Top left: phase map recorded right after the establishment of a stationary temperature field in the cell. Top right: colormap of the computed temperature in the liquid. Bottom left: vertical temperature profiles in the liquid. Bottom right: horizontal temperature profiles in the liquid.

Q7

538 where  $n_{1,T} = \partial n_1 / \partial T|_{w_1, w_2} = -0.00447$  is the thermal contrast factor  
 539 at wavelength  $\lambda_1$ .<sup>60</sup> In Fig. 10, we observe a strong curvature of the  
 540 temperature field approaching the edges of the cell. The temperature  
 541 difference between the top and the bottom of the cell is close to 10 °C  
 542 in the center of the cell but significantly smaller at the Quartz walls.  
 543 The temperature profiles along several vertical and horizontal lines  
 544 are plotted in Fig. 10.

## 545 B. Soret coefficients

546 The refractive index difference between the top and the bot-  
 547 tom of the cell ( $n_{ib}$ )<sub>*i*</sub> for both wavelengths and the corresponding  
 548 Soret coefficients obtained by using the 7 different data processing  
 549 schemes are reported in Table V. We do not report data for cell 3 in  
 550 the present paper, as it was previously studied in detail.<sup>12,26,32,33,48,54</sup>

551 In Table V, outlier data points corresponding to  $S'_{T,1}$  or  $S'_{T,2}$   
 552 and deviating of more than 2 standard deviations from the mean  
 553 coefficients are indicated by a \* superscript. Based on this set of  
 554 results, we report in Table VI the mean Soret coefficients obtained  
 555 in the present study, together with the coefficients found in the  
 556 literature, including coefficients obtained by OBD,<sup>52</sup> by a previ-  
 557 ous analysis of DCMIX1 data<sup>32,54</sup> and by combination of SST and  
 558 thermogravitational column experiments (SST + TC).<sup>55</sup>

559 For cells 1–4, at least 2 Soret coefficients were obtained with  
 560 a reasonable accuracy. For cell 5, the experimental data did not  
 561 allow identifying accurately the Soret coefficients. We provide the  
 562 coefficients obtained for cell 5, but we acknowledge that given the  
 563 amplitude of the standard deviation, these values should be taken  
 564 with caution. The first observation is that, in all systems, the heavier

565 component, tetralin, showed a positive Soret effect, which means  
 566 that it concentrated at the cold side of the cell. Moreover, the magni-  
 567 tude of the separation of tetralin is larger than that of the two other  
 568 components (except in cell 5). The systems studied through the first  
 569 three cells are located close to the three corners of the ternary con-  
 570 centration diagram (see Table I), where one of the components is  
 571 more concentrated than the other two ( $n_{C12}$  in cell 1, *IBB* in cell  
 572 2, and *THN* in cell 3). The comparison of the results obtained for  
 573 these cells provides an illustration of the complexity of thermodiffu-  
 574 sion in multicomponent mixtures. We do not observe any obvious  
 575 correlation between the concentration of the components and the  
 576 amplitude of the Soret coefficients. In the present study, we obtained  
 577 a negative coefficient for *IBB*, but this observation is not confirmed  
 578 by previous experimental studies. In cell 2,  $S'_{T,2}$  is larger than  $S'_{T,3}$ ,  
 579 while in cells 1 and 3,  $S'_{T,3}$  is larger. The separation of tetralin is  
 580 significantly larger in cells 4 and 5 than in cells 1–3.

## 581 1. Comparison of data processing approaches

582 As indicated in Eq. (2), the steady state thermodiffusive con-  
 583 centration fields are proportional to the temperature field in the  
 584 cells. Due to the curvature of the temperature field, the refractive  
 585 index differences measured by interferometry tend to underestimate  
 586 the Soret separation. Data processing sequences DP1 and DP2 used  
 587 identical image processing algorithms and mathematical models, the  
 588 only difference being the tomographic reconstruction of the refrac-  
 589 tive index fields. Thus, the refractive index differences, and the Soret  
 590 coefficients, computed by DP2 are significantly larger than the ones  
 591 obtained by DP1.

592 **TABLE V.** Refractive index differences at both wavelengths and Soret coefficients  
593 obtained with the 7 data processing sequences of Table II. Components 1, 2, and 3  
594 are, respectively, THN, IBB, and nC<sub>12</sub>; C is the cell number; DP is the data processing  
595 scheme according to Table II; and run is the run reference according to Table I. \*  
596 superscript denotes outlier data points.

597			$-(n_{ib})_1$	$-(n_{ib})_2$	$S_{T'1}$	$S_{T'2}$	
598	C	DP	$10^{-4}$		$10^{-4} \text{ K}^{-1}$		
599	1	1	16	6.103	5.929	9.41	-5.35
600			21	6.086	5.921	10.07	-6.53
601	2	16	16	6.852	6.662	11.04	-6.76
602			21	6.836	6.645	10.85	-6.54
603	3	16	16	6.107	5.952	11.0	-8.1
604			21	6.119	5.946	9.5	-5.5
605	4	16	16	5.78	5.73	*18.8	*-2.24
606			21	5.77	5.69	*15.8	*-17.1
607	5	16	16	6.22	6.07	12.2	-10.0
608			21	6.26	5.98	*1.0	*9.7
609	6	11	11	6.161	5.924	4.61	3.17
610			16	5.790	5.630	9.33	-5.79
611			21	5.710	5.520	6.64	-1.21
612	7	16	16	6.314	6.065	4.2	4.17
613			21	6.181	5.947	4.9	2.7
614	2	17	17	5.133	4.978	6.55	-4.01
615			02	5.199	5.041	6.58	-3.98
616	1	22	22	5.148	5.004	7.11	-4.91
617			27	5.172	5.023	6.93	-4.60
618		07r	07r	5.202	5.042	6.50	-3.83
619	17	02	02	5.714	5.545	7.45	-4.73
620			02	5.757	5.578	7.09	-4.09
621	2	22	22	5.730	5.564	7.63	-5.00
622			27	5.742	5.578	7.76	-5.20
623		07r	07r	5.780	5.622	8.14	-5.78
624	3	2	2	5.2428	5.087	6.8	-4.3
625			17	5.2307	5.063	6.2	-3.3
626			22	5.2122	5.062	7.0	-4.6
627			27	5.2272	5.073	6.9	-4.4
628	17	02	02	5.04	4.87	5.9	-3.0
629			02	4.92	4.84	9.3	-8.9
630	4	22	22	4.97	4.82	6.3	-3.8
631			27	4.96	4.84	7.6	-5.9
632		27 r	27 r	4.93	4.85	*9.8	*-9.6
633	2	17	17	5.06	4.81	*2.1	*3.3
634			17	-5.01	-4.79	*2.7	*2.2
635	5	22	22	-4.99	-4.81	4.8	-1.3
636			27	-4.99	-4.78	3.4	0.9
637		27r	27r	4.98	4.86	7.8	-6.3
638	6	2	2	5.613	5.416	6.0	-2.4
639			12	5.359	5.192	6.08	-3.0
640		17	17	5.359	5.192	6.59	-3.78

642 **TABLE V. (Continued.)**

643			$-(n_{ib})_1$	$-(n_{ib})_2$	$S_{T'1}$	$S_{T'2}$	
644	C	DP	$10^{-4}$		$10^{-4} \text{ K}^{-1}$		
645	7		2	5.286	5.092	5.09	-1.41
646			7	5.251	5.063	5.31	-1.82
647			12	5.172	5.067	9.00	-8
648			22	5.241	5.067	5.91	-2.82
649	4	3	4	21.022	20.431	34.9	-27.8
650			19	20.898	20.312	34.8	-27.8
651		24	20.845	20.248	33.4	-25.6	
652	6	4	4	20.719	20.063	27.39	-15.68
653			19	19.9621	19.3060	24.0	-11.0
654		24	19.5198	18.9097	26.6	-16.1	
655	7	4	4	20.8220	20.2560	36.79	-31.28
656			19	20.6856	20.0665	30.90	-21.60
657		24	20.9056	20.3094	34.17	-26.76	
658	5	1	15	18.65	18.10	47.31	-52.29
659			20	19.29	18.73	50.84	-57.27
660			5	19.13	18.71	79.49	-105.4
661			25	18.80	18.25	48.64	-54.30
662	2	15	15	20.96	20.34	55.32	-62.39
663			20	22.16	21.52	57.41	-64.18
664		5	20.89	20.54	110.44	-54.22	
665		25	21.23	20.69	70.55	-87.46	
666	3	5	5	19.815	19.193	42.2	-42.1
667			15	19.105	18.488	37.1	-34.5
668		20	19.021	19.169	*200.0	*-308	
669		25	19.442	18.728	19.2	-4.2	
670	6	5	5	*18.27	*17.11	*6.69	*-1.15
671			10	19.561	18.915	34.7	-29.9
672		15	17.46	17.01	57.9	-71.7	
673	7	5	5	18.65	17.93	11.3	7.9
674			10	18.5	17.78	8.9	11.7
675			15	18.3	17.59	11.0	7.9
676			20	18.21	17.49	9.0	11.1
677		25	18.48	17.82	23.0	-11.9	

680 DP5 results in the most scattered Soret coefficients. In DP5, the  
681 optical phases of the experimental data were collected during the  
682 diffusion step of the experiments. Due to the alignment of the inter-  
683 ferometer in wide fringe configuration, the images collected during  
684 this step of the runs only contain a few fringes, and the Fourier  
685 algorithm results in noisy phase signals.

686 DP3 and DP7 are based on very different mathematical mod-  
687 eling of the diffusive processes but implement similar image pro-  
688 cessing algorithms. The coefficients obtained through these two data  
689 processing sequences are very consistent. This seems to indicate that  
690 the influence of the image processing algorithms is more critical than  
691 the mathematical modeling of the experiments.

**TABLE VI.** Average Soret coefficients obtained in this study, compared with literature data.<sup>32,52,54,55</sup> Components 1, 2, and 3 are, respectively, *THN*, *IBB*, and *nC<sub>12</sub>*. \*\* superscript denotes corrected data.

C	References	$S'_{T1}/10^{-4}$ (K <sup>-1</sup> )	$S'_{T2}/10^{-4}$ (K <sup>-1</sup> )	$S'_{T3}/10^{-4}$ (K <sup>-1</sup> )	
1	This study	8.6 ± 2.8	-3.8 ± 4.8	-4.8 ± 2	
	TC + SST <sup>55</sup>	5.4 ± 0.7	3.2		
	OBD <sup>52</sup>	5.8	3.9	-9.0	
	DCMIX1 <sup>54</sup>	6.02 ± 0.4	-0.42 ± 0.2		
2	This study	6.7 ± 1.2	-4.1 ± 2.0	-2.6 ± 0.8	
	DCMIX1 <sup>32</sup>	-7.42 (+7.42 <sup>**</sup> )	-0.59 (-5.90 <sup>**</sup> )		
	TC + SST <sup>55</sup>	3.1 ± 0.6	2.9		
	OBD <sup>52</sup>	4.1	0.2	-4.4	
3	Benchmark <sup>12</sup>	12.8 ± 0.4	-5.8 ± 0.3	-7	
	4	This study	31.40 ± 4.5	-22.6 ± 7	-8.8 ± 2.5
		TC + SST <sup>55</sup>	19 ± 2	1.0	
		OBD <sup>52</sup>	21.7	-1.4	-20.3
DCMIX1 <sup>54</sup>		21.5 ± 0.6	-4.94 ± 0.4		
5	This study	44.56 ± 27	-44.8 ± 44	1.34 ± 17	
	TC + SST <sup>55</sup>	15 ± 4	6		
	OBD <sup>52</sup>	19.5	-1.7	-17.7	

In DP7, the mathematical modeling of the diffusive processes is simplified and can only be used if the Soret separation actually attains steady state at the end of the Soret phase of the runs.

## 2. Analysis of errors on the Soret coefficients

In Fig. 11, we have plotted in a  $S'_{T1}$ - $S'_{T2}$  space the Soret coefficients obtained through the 7 data processing sequences together with the coefficients found in the literature.

A first observation is that, as discussed in Ref. 29, the coefficients obtained with different data processing methods are aligned in the  $S'_{T1}$ - $S'_{T2}$  space. The error of the Soret coefficients has a remarkable property: instead of forming a radially uniform scattering cloud around the solution point  $\{S'_{T1}, S'_{T2}\}$ , it forms a very elongated ellipsoid, practically degenerated into a line. This means that all data processing sequences of Table II lead to consistent optical analysis of the experimental data. The dispersion on the obtained Soret coefficients is due to the conversion of optical quantities to concentration quantities. This step, in Eq. (7), requires inverting the matrix of optical contrast factors. This matrix is quite ill-conditioned, and the inversion amplifies a low optical noise into a large uncertainty in the concentrations. The orientation of the line in the  $S'_{T1}$ - $S'_{T2}$  space is defined by the properties of the contrast factor matrix. In Ref. 61, it has been shown that the directions of the major and the minor axis of the uncertainty ellipsoid are given by the right-singular vectors of the contrast factor matrix. Based on this observation, it appears that DCMIX1 experimental data do not allow retrieving the ternary Soret coefficients with the same accuracy as for typical binary mixtures. However, these data provide a linear correlation between the

Soret coefficients. By writing this correlation as

$$S'_{T2} = AS'_{T1} + B, \quad (11)$$

we obtain the values of parameters A and B provided in Table VII.

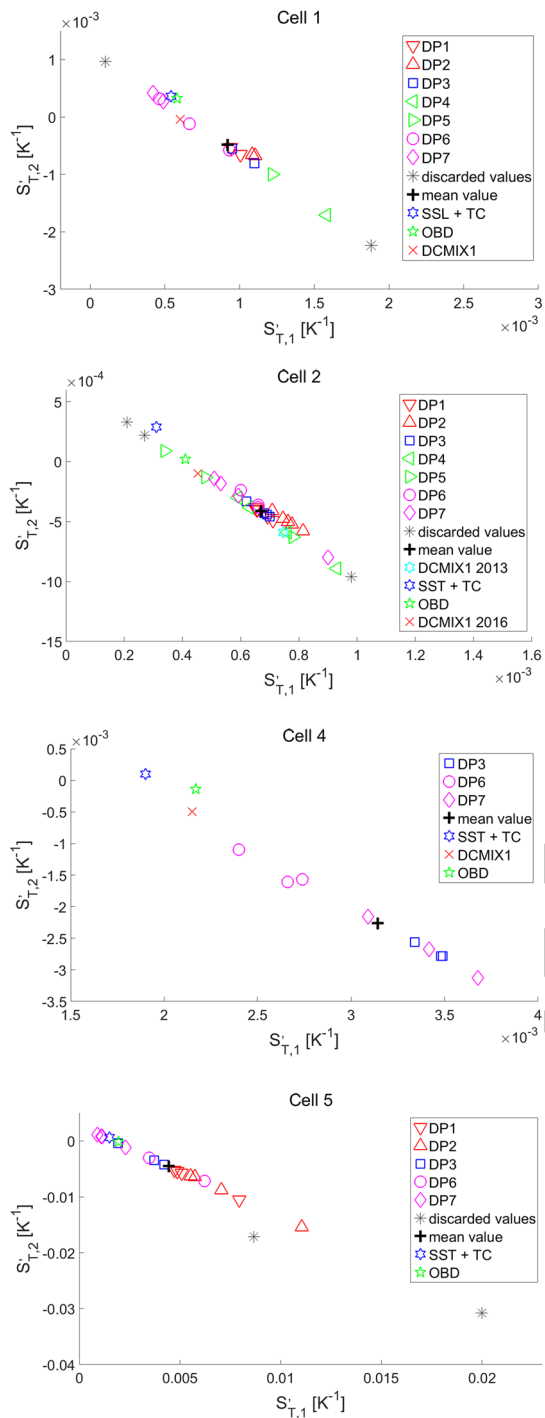
This linear correlation corresponds essentially to the result of a single-color experiment. The second detection color narrows the solution space down from a straight line to a line segment, whose length depends on the condition number of the contrast factor matrix.

The consistency of the obtained results shows that, in general, all data processing sequences of Fig. 4 and Table II can reliably be used for the interpretation of ternary thermodiffusion experiments and we cannot point out clear criteria for preferring one data processing methodology over the others. On the other hand, such criteria may appear from a particularity of the raw data itself. The choice of a particular data processing methodology must be made on a case by case basis, depending on the characteristics of the experimental data.

## 3. Comparison with literature data

The comparison of our results with literature data,<sup>32,52,54,55</sup> as summarized in Fig. 11, shows that the coefficients found in previous publications are also located on the lines defined by Eq. (11). The coefficients of Refs. 32 and 54 were obtained from previous analysis of DCMIX1 data and computed using similar contrast factor matrices. These coefficients therefore unsurprisingly display the same trend as our results. Although, in the previous analysis, the authors did not notice and describe the scattering of  $S'_{T1}$  and  $S'_{T2}$  because





769 **FIG. 11.** Comparison of Soret coefficients with literature data, for DCMIX1 cells 1,  
770 2, 4, and 5. The coefficients were obtained through data processing sequences  
771 DP1 to DP7 and compared with literature data, including coefficients obtained by  
772 the Optical Beam Deflection (OBD) technique,<sup>52</sup> by a previous analysis of DCMIX1  
773 data,<sup>32,54</sup> and by combination of sliding symmetric tubes and thermogravitational  
774 column experiments (SST + TG).<sup>55</sup> All the obtained coefficients are aligned in the  
775  $S'_{T,1}-S'_{T,2}$  space.

776 **TABLE VII.** Coefficients of the linear correlation between the Soret coefficients  
777 obtained in this study.  
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Cell	A	B
1	-1.6877	0.0011
2	-1.5856	0.0007
4	-1.5449	0.0026
5	-1.6347	26.2379

779 the conversion of refractive index into concentration in their algo-  
780 rithm was applied at an early stage, which resulted in overlooking  
781 the effect.  
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## V. CONCLUSIONS

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The Soret coefficients of a series of five ternary systems were performed under microgravity conditions aboard the International Space Station in the frame of the DCMIX1 experiment. In the present paper, we have detailed the experimental setup, the procedure, and the experimental data analysis. We have provided an extended review of the different possible data processing schemes used in the interpretation of digital interferometric ternary thermodiffusion experiments. We have shown that different choices of image processing algorithm and mathematical modeling of the experiments are possible and lead to consistent results. We have observed that the measured Soret coefficients are aligned in the  $S'_{T,1}-S'_{T,2}$  space and that there remains an indetermination on the values of the measured Soret coefficients due to the ill-conditioned matrix of optical contrast factors. We have derived a linear correlation between the Soret coefficients for each ternary system. These correlations allow for an experimental validation of the Soret coefficients measured by OBD<sup>52</sup> and by the combination SST + TG<sup>55</sup> in ground conditions by comparison with the results of the microgravity DCMIX1 experiment.

From the comparison with literature data, we can conclude the consistency of the data obtained from the SODI instrument by different data processing approaches. Besides, we have compared our results with coefficients obtained in ground laboratories, by SST + TC in Ref. 55 or by OBD in Ref. 52. Those coefficients were computed using density and refractive index or refractive index at two different wavelengths (405 and 635 nm), respectively, for the concentration measurements. These techniques are therefore based on different contrast factor matrices, which provide some advantages for this particular system.

Nevertheless, all the coefficients, although measured with very different experimental techniques, using a variety of data processing approaches, and computed with different sets of contrast factors, are all located on the lines of Fig. 11. This observation suggests that the results of DCMIX1 allow for an experimental validation of the coefficients measured under gravity conditions in Refs. 52 and 55. As a general result, the Soret coefficients can be fixed in the direction of the short axis of the confidence ellipsoid with a high accuracy. How far they can be narrowed down in the perpendicular direction of the long axis very strongly depends on the contrast factor matrix and, hence, on the particular ternary mixture and the

employed experimental technique. For a mixture containing both aromatic and aliphatic compounds, it is advantageous to choose one wavelength in the blue, close to the UV-absorption of the delocalized  $\pi$ -electrons.<sup>62</sup> The DCMIX1 system belongs to this class of mixtures. But this advantage may be gone for systems without an aromatic compound. Also, the combination of density and refractive index detection, as employed in the thermogravimetric column technique, can in certain cases profit from superior contrast factor matrices. Unfortunately, no perfect experimental technique exists that could cover all possible mixtures, and a change of the detection wavelengths is not feasible for the microgravity experiments.

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