

Meander-Line Polarizer for Omnidirectional Antenna

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Abstract— Meander-line polarizer for a half-wave vibrator is presented. Researched antenna was simulated and prototype was manufactured. The comparison of the theoretical and experimental data for investigated antenna (axial ratio) was produced. Influence of polarizer on half-wave vibrator matching characteristics was researched.

Keywords — polarizer; meander-line; axial ratio.

I. INTRODUCTION

Nowadays compact omnidirectional circularly polarized antenna is required for different tasks such as radio navigation, satellite and wireless communications. One of the ways to obtain the circular polarization is the use of polarizers. The elementary polarizer type convenient for research, simulation and realization is a meander-line structure. Small thickness of the metal layer allows getting flat and thin polarizer. This design is especially suitable for half-wave vibrator antennas, where the polarizer should have a cylindrical shape. Thin structure allows changing shape easily within certain limits.

Meander-line polarizer was described in the article [1], where possibility of cylindrical shape polarizer creation was researched, and the polarizer operation principle was described. The dimensions for four-layer meander-line polarizers and axial ratio (AR) measurement results are shown in [1] also. Optimization of one-layer polarizer was produced by using presented approach and modern CAD software.

II. MEANDER-LINE DESIGN

Meander-line polarizer is a set of thin metal structures in meander form (Fig. 1). Its operating principle is detailed and calculation equation for polarizer sizes are presented in articles [2,3].



Fig. 1. Meander-line.

For flat polarizer realization, several meander-lines are located at a defined distance (s) from each other in one plane, as shown in Fig. 2. The number of periods (n) and number of meander-lines (N) are chosen considering an illuminator sizes and a distance from illuminator to polarizer.

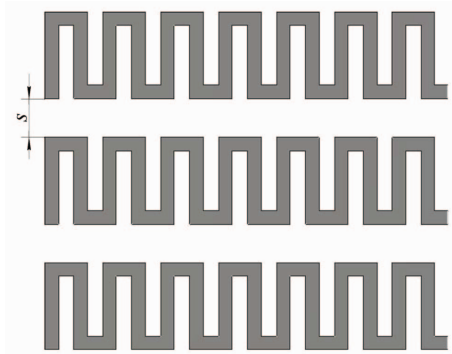


Fig. 2. Plane meander-line polarizer.

The calculated sizes of the meander-line and polarizer have been optimized for one-layer operating at central frequency of 2.4-2.5 GHz band. One-layer polarizer can be used for a narrow-band applications, and multilayer polarizers allow to increase operation frequency band as described below in chapter IV.

III. MEANDER-LINE POLARIZER DESIGN

For cylindrical polarizer the supporting cylinder of required radius was made of foamed polystyrene. This material has dielectric constant $\epsilon \approx 1.5$. The dielectric permittivity does not influence the antenna and polarizer characteristics as experimental results show. The structure of several meander-lines was fabricated of the copper-foil deposited polyethylene terephthalate (PET) 0.25 mm thick. This material is flexible, that allows getting any required shape. The meander-line structure is inclined at angle 45° for left-hand or -45° for right-hand circular polarization and is wrapped around dielectric cylinder (Fig. 3).

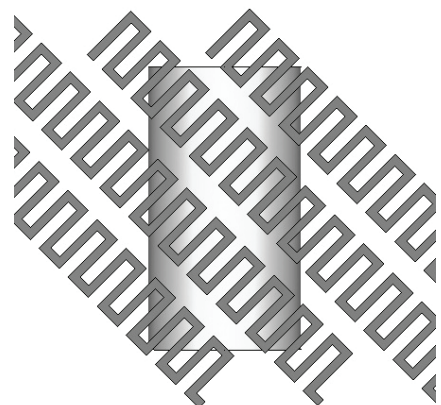


Fig. 3. Plane meander-line polarizer.

A half-wave electric vibrator is used as a polarizer illuminator and is placed in the cylinder center. The vibrator produces the torus shape radiation pattern (RP). Thus, the polarizer is supposed to be placed at the same distance from the antenna in all directions. The distance between the meander-lines and their number aren't limited in a flat polarizer (at a known size h). For cylindrical polarizer these parameters directly depend on cylinder circumference (diameter D). Thus, the distance between meander-lines (s) is calculated as follows:

$$s = \sqrt{\left(\frac{D \cdot \pi}{N}\right)^2 \frac{1}{2} - h}$$

The presented equation takes into account that the distance between the last and the first meander lines will be equal to s at structure wrapping on the cylinder. The polarizer prototype was fabricated according to calculations results (Fig.4).

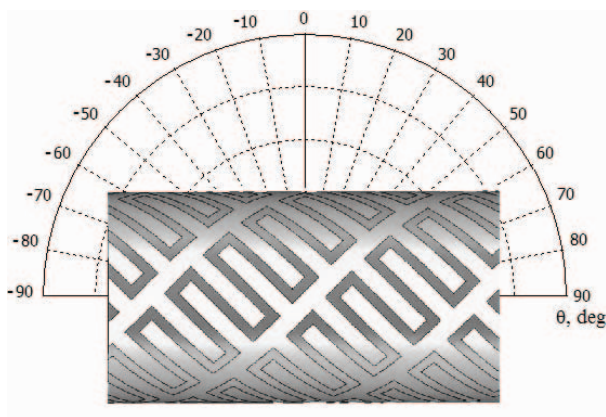


Fig. 4. Cylindrical meander-line polarizer.

IV. RESULTS AND DISCUSSION

The following characteristics are obtained after numerical parameters optimization (Fig.5-8).

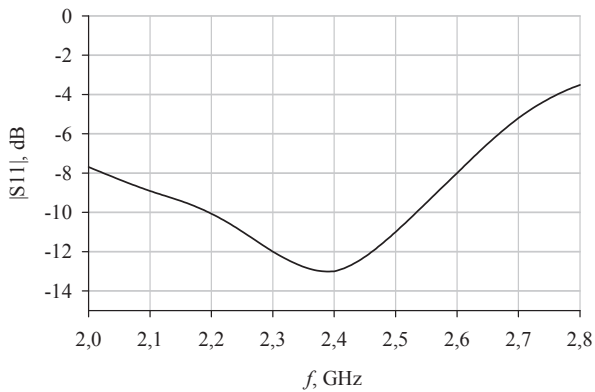


Fig. 5. Calculated S_{11} parameters of vibrator antenna with a polarizer.

The vibrator antenna with a polarizer is properly matched within the necessary frequency range. S_{11} parameter of the same vibrator antenna without polarizer is presented in Fig.6.

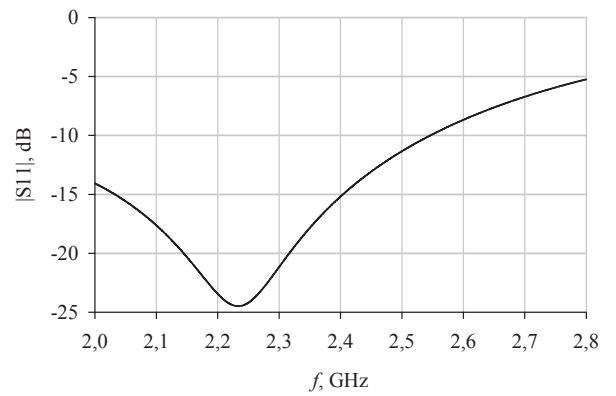


Fig. 6. Calculated S_{11} parameter of vibrator antenna without a polarizer.

The vibrator antenna without a polarizer has better matching characteristics, but the central working frequency is 2.245 GHz. The polarizer shifts the working frequency range. However, the prototype of the antenna with a polarizer provides better matching than the CAD model.

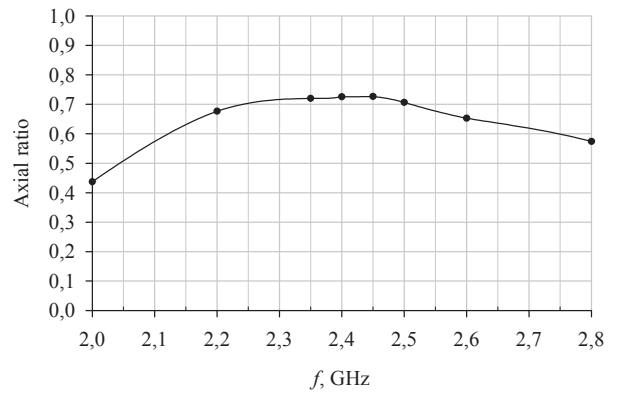


Fig. 7. Calculated axial ratio of vibrator antenna with a polarizer.

Axial ratio corresponding to the radiation pattern maximum is not less than 0.7 within the working frequency range, i.e. the cross-polarization level is less than -14.5 dB (Fig.8).

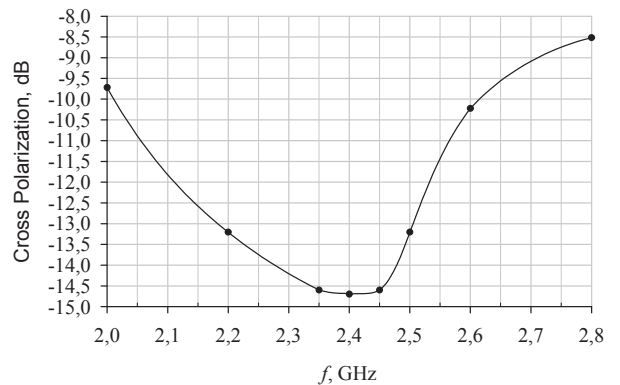


Fig. 8. Calculated cross polarization of vibrator antenna with a polarizer.

As already told in chapter II, it is possible to expand a working frequency range by using several meander-line polarizers, placed one above the other (Fig.9).



Fig. 9. Segment of 3-layer polarizer structure.

Axial ratio of circular three-layer polarizer is shown in Fig. 10.

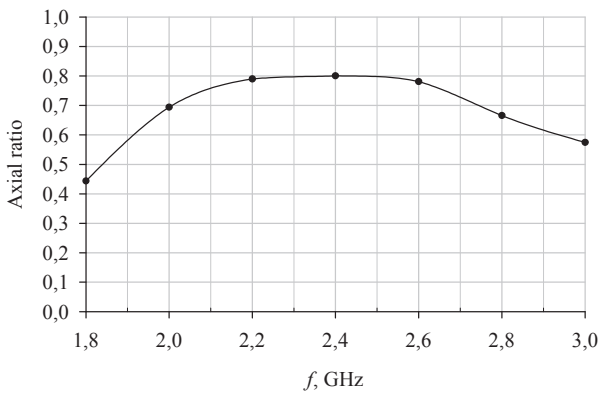


Fig. 10. Calculated axial ratio of vibrator antenna with a three-layer polarizer

Several layers polarizer allows to expand the working frequency range up to more than 30% and to increase axial ratio for center frequency up to 0,8. Cross-polarization level is as low as -19 dB (Fig. 11).

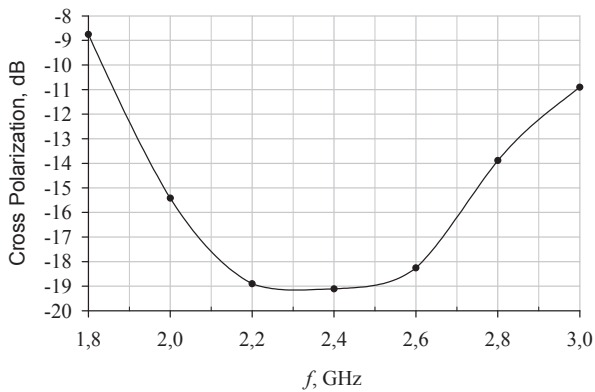


Fig. 11. Calculated cross polarization of vibrator antenna with a three-layer polarizer.

V. MEASUREMENTS

Based on the calculation result two models of antennas with a polarizer for left and right circular polarizations were manufactured (Fig. 12).

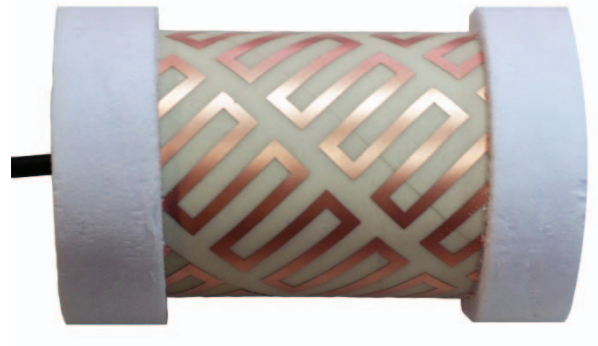


Fig. 12. Antenna prototype.

Cylinder dimensions are diameter - 65 mm, length - 120 mm.

Measurements were carried out in anechoic chamber in far field. Results are presented in Fig.13-16.

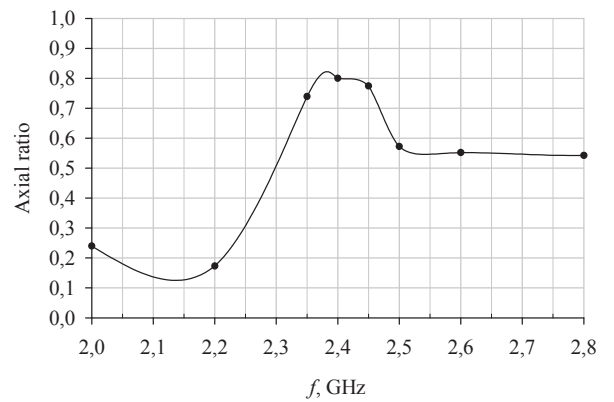


Fig. 13. Measured axial ratio of vibrator antenna with a polarizer (left-hand polarization).

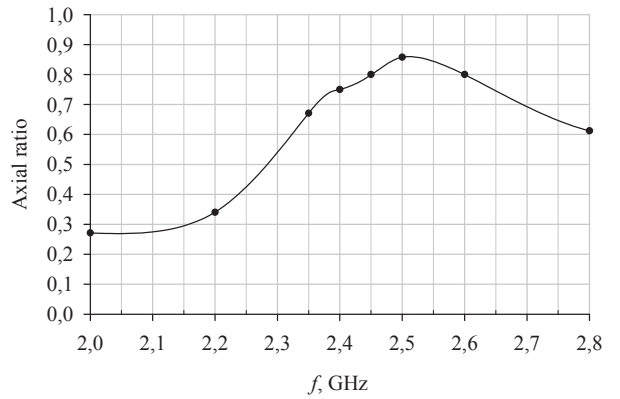


Fig. 14. Measured axial ratio of vibrator antenna with a polarizer (right-hand polarization).

Axial ratio measurement results differ from the simulation. This is partly connected to the material losses unaccounted in the calculations. Prototype manufacturing inaccuracy also influences antenna characteristics. The last fact explains differences between AR for the left and right

polarizations. Nevertheless, axial ratio values in the working frequency range are similar.

Axial ratio angular dependence at the central frequency (2.445 GHz) is presented in Fig. 15. Angular scale corresponds to Fig. 4.

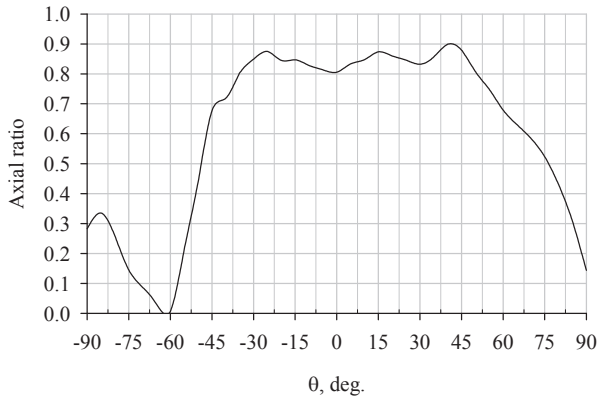


Fig. 15. Measured axial ratio angular dependence at 2.445 GHz.

Axial ratio value is stable in $\pm 45^\circ$ angle range. Meander-lines projection changes with angle increasing. This fact leads to significant axial ratio reduction at angles more than 45° . However, half-wave vibrator antenna employment makes no sense for directions $\theta > \pm 45^\circ$ due to low level of radiation pattern.

Radiating pattern of vibrator antenna with polarizer is insignificantly tilted due to asymmetry of half-wave vibrator feed point and feed line (Fig. 14).

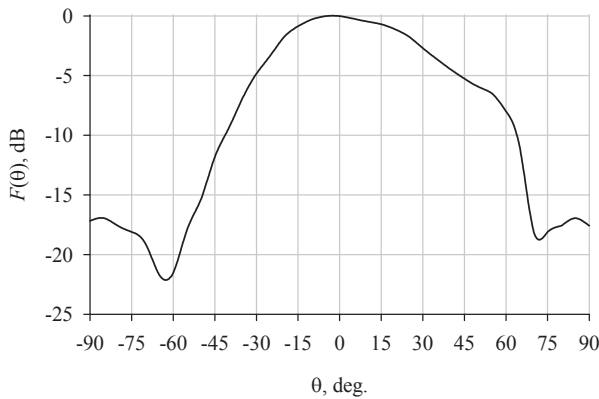


Fig. 16. Measured radiation pattern of vibrator antenna with a polarizer at 2.445 GHz.

VI. CONCLUSION

Presented polarizer type can be used together with half wave vibrator antenna to transform linear polarization to circular. Meander-lines arrangement relative to the antenna allows producing of both right-hand and left-hand circular polarizations. Results of modeling and experimental measurements demonstrate the possibility of production and practical application of such polarizer.

References

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