# Enhanced Degradation and Mineralization <br> of Bisphenol A by Hybrid Process <br> Using Hydrodynamic-Acoustic Cavitation 

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## Кавитационная активация процессов деструкции

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## TEXT A

A number of studies have been devoted to the degradation of BPA under the influence of cavitation (Table S 1). Torres R. A. et al. [1]a chemical compound largely used in the plastics industry, can end up in aquatic systems, which it disturbs by its endocrine disrupting effect (EDE studied the degradation of BPA under ultrasound exposure in various experimental conditions. The optimal degradation efficiency for BPA with a concentration of $118 \mu \mathrm{M}$, was achieved through ultrasound treatment at 300 kHz and 80 W , utilizing oxygen as the saturating gas. This resulted in the complete removal of BPA within 90 minutes. However, even after treatment for 9 hours a reduction of COD by $50 \%$, and TOC by $20 \%$ has been achieved. Kitajima et al. [2]3-dihydro-2-methylbenzofuran also studied the ultrasonic degradation of BPA $(491 \mathrm{kHz}, 120 \mathrm{~W})$ in an oxygen medium and observed complete removal of the compound within 2.5 hours of treatment. They also elucidated the role of hydroxyl radicals formed by water dissociation in the oxidative process. Deggelmann M. et al.[3] performed BPA degradation under high pressure HC and achieved $50 \%$ removal in 30 minutes of treatment, although the initial contaminant concentration was low $(0.25 \mu \mathrm{M})$. Lu G. et al. [4] investigated the prospects of using low-pressure HC ( 3 bar) for BPA degradation (its concentration decreased by $27.6 \%$ in 3 hours of treatment).

The possibility of combining cavitation with AOPs has been considered. For instance, electrochemical oxidation combined with AC reduced the concentration of BPA by $90 \%$ in 30 minutes of treatment [5] an endocrinic disruptor, which is widely used in plastic production. Due to its endocrine disrupting effects on aquatic (micro-. Using the sono-Fenton process, $94 \%$ of the BPA was removed in 40 minutes of treatment [6]. A study by Torres R. A. et al. [1]a chemical compound largely used in the plastics industry, can end up in aquatic systems, which it disturbs by its endocrine disrupting effect (EDE reported that complete mineralization of BPA can be achieved by combining ultrasound ( 300 kHz ) with $\mathrm{Fe}(\mathrm{II})$ and UV (254 nm). Under these conditions, the treatment for 2 hours resulted in a reduction of COD by $96 \%$, and TOC by $79 \%$.

Currently, many studies focus on sulfate radical-based AOPs (SR-AOPs), where persulfates (PS) are used as ROS precursors. This process produces sulfate anion radicals in solution, which have a high oxidative capacity, longer lifetime in solution, and greater selectivity [7,8]. Choi J. et al. [9]in order to oxidize BPA at the water treatment, an economical treatment method is required. This study
was the first study to apply hydrodynamic cavitation/persulfate (HC/PS studied the oxidation of BPA by PS under HC conditions. At an optimum pressure of 5 bar and an elevated temperature of $50^{\circ} \mathrm{C}$, the removal efficiency of BPA reached $81.3 \%$ in 2 hours of treatment [9]in order to oxidize BPA at the water treatment, an economical treatment method is required. This study was the first study to apply hydrodynamic cavitation/persulfate (HC/PS. Darsinou B. et al. [10] demonstrated that PS activation can be achieved using AC at 20 kHz , resulting in complete degradation of BPA in 90 minutes. After 8 hours of treatment, the reduction of TOC reached $60 \%$.

Table S 1. Summary of the literature on the degradation of BPA using cavitation processes

| Treatment approach | Type of reactor | [BPA], $\mu \mathrm{M}$ | Optimized condition | Rate Constant | $\begin{gathered} \hline \text { Removal/ } \\ \text { COD/ } \\ \text { TOC, \% } \end{gathered}$ | Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AC | Reactor with a piezo-electric disk (at the bottom) | 118 | $\begin{aligned} & \mathrm{V}=0.3 \mathrm{~L}, 300 \mathrm{kHz}, 80 \mathrm{~W}, \\ & \mathrm{~T}=20^{\circ} \mathrm{C}, \mathrm{t}=9 \mathrm{~h}, \end{aligned}$ |  | 100/50/20 | [1] |
| AC | Concave PZT transducer | 219.3 | $\begin{aligned} & \mathrm{V}=0.05 \mathrm{~L}, \\ & 491 \mathrm{kHz}, 120 \mathrm{~W} . \mathrm{T}=20^{\circ} \mathrm{C}, \\ & \mathrm{t}=2.5 \mathrm{~h}, \mathrm{O}_{2} \text { media } \end{aligned}$ | $7.3 \cdot 10^{-4} \mathrm{~s}^{-1}$ | 100 | [2] |
| HC | HC, <br> Nozzle | 0.25 | $\begin{aligned} & \mathrm{V}=0.5 \mathrm{~L}, 1.7 \mathrm{~mm} \text { nozzle, } \\ & \mathrm{P}=25 \mathrm{bar}, \mathrm{pH}=6, \\ & \mathrm{~T}=20^{\circ} \mathrm{C}, \mathrm{t}=0.5 \mathrm{~h}, \end{aligned}$ |  | 50 | [3] |
| HC | $\mathrm{HC},$ <br> Orifice plate, | 43.8 | $\mathrm{V}=20 \mathrm{~L}, \mathrm{P}=3 \mathrm{bar},$ <br> Diameter of each hole 1 mm , No. of holes 61. $\mathrm{pH}=6$, $\mathrm{T}=35^{\circ} \mathrm{C}, \mathrm{t}=3 \mathrm{~h} .$ | $2.12 \mathrm{~s}^{-1}$ | 27.6 | [4] |
| AC + Fenton | ULTRAsonikTM 104X bath | 109.6 | $\begin{aligned} & \mathrm{V}=0.25 \mathrm{~L}, 43-47 \mathrm{kHz}, \\ & 500 \mathrm{~W} \cdot \mathrm{pH}=4, \mathrm{~T}=25^{\circ} \mathrm{C}, \\ & \mathrm{t}=1 \mathrm{~h},\left[\mathrm{Fe}^{+}\right]=9 \mu \mathrm{M}, \\ & {\left[\mathrm{H}_{2} \mathrm{O}_{2}\right]=25 \mu \mathrm{M} .} \end{aligned}$ |  | 100 | [6] |
| AC | Reactor with a piezo-electric disk (at the bottom) | 118 | $\begin{aligned} & \mathrm{V}=0.3 \mathrm{~L}, 300 \mathrm{kHz}, 80 \mathrm{~W} \\ & \mathrm{~T}=20^{\circ} \mathrm{C}, \mathrm{t}=7 \mathrm{~h}, \mathrm{pH} 3 . \end{aligned}$ |  | 100/50/17 | [11] |
| AC+Photo $+\mathrm{Fe}^{2+}$ | Reactor with a piezo-electric disk (at the bottom) | 118 | $\begin{aligned} & \mathrm{V}=0.3 \mathrm{~L}, 300 \mathrm{kHz}, 80 \mathrm{~W}, \\ & \mathrm{~T}=20^{\circ} \mathrm{C}, \mathrm{t}=2 \mathrm{~h}, \mathrm{pH} 3 . \\ & \mathrm{Fe}^{2+}=100 \mu \mathrm{M} . \\ & \text { UVC } 254 \mathrm{~nm}, \mathrm{O}_{2} \text { media } \end{aligned}$ |  | 100/96/79 | [11] |
| AC+electrochemical treatment | Ultrasound generator with a sonotrode S 14L2D, titanium | 4.38 | $\begin{aligned} & \mathrm{V}=0.5 \mathrm{~L}, 24 \mathrm{kHz}, 80 \mathrm{~W} . \\ & \mathrm{T}=20^{\circ} \mathrm{C}, \mathrm{t}=30 \text { min. two } \end{aligned}$ <br> boron doped diamond electrodes ID $=8.1 \mathrm{~cm}$, $\left[\mathrm{Na}_{2} \mathrm{SO}_{4}\right]=30 \mathrm{mM}$ | 0,043 $\mathrm{min}^{-1}$ | 90 | [5] |
| AC+magnetic biochar $+\mathrm{H}_{2} \mathrm{O}_{2}$ | Sonicator VCX 750 with a titanium probe | 100 | $\begin{aligned} & \mathrm{V}=0.2 \mathrm{~L}, 20 \mathrm{kHz}, 750 \mathrm{~W}, \\ & \mathrm{~T}=20^{\circ} \mathrm{C}, \mathrm{t}=40 \mathrm{~min} . \\ & \text { Catalyst dose }=1 \mathrm{~g} / \mathrm{L}, \\ & {\left[\mathrm{H}_{2} \mathrm{O}_{2}\right]=10 \mathrm{mM} .} \end{aligned}$ |  | 94 | [12] |
| $\overline{\mathrm{AC}+\mathrm{UVA}+\mathrm{TiO}_{2}}$ | Fabricated stainless-steel transducer module (Fulltech, Taiwan) | 4.38 | $\begin{aligned} & \mathrm{V}=1 \mathrm{~L}, 35 \mathrm{kHz}, 100 \mathrm{~W} . \\ & \mathrm{T}=25^{\circ} \mathrm{C}, \mathrm{t}=1 \mathrm{~h} . \\ & \mathrm{TiO}_{2}=0.05 \mathrm{~g} / \mathrm{L} \text { UVA } 350 \mathrm{~nm} . \end{aligned}$ | $\begin{aligned} & 8.75 \times 10^{-2} \\ & \min ^{-1} \end{aligned}$ | 100 | [13] |


| Treatment approach | Type of reactor | [BPA], $\mu \mathrm{M}$ | Optimized condition | Rate Constant | $\begin{gathered} \hline \text { Removal/ } \\ \text { COD/ } \\ \text { TOC, \% } \end{gathered}$ | Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AC+PS | Branson 450 horntype | 21.9 | $\begin{aligned} & \mathrm{V}=0.12 \mathrm{~L}, \\ & 20 \mathrm{kHz}, 450 \mathrm{~W}, \mathrm{~T}=30^{\circ} \mathrm{C}, \\ & \mathrm{t}=8 \mathrm{~h}, \mathrm{pH} 6 . \mathrm{PS}=500 \mathrm{mg} / \mathrm{L} \end{aligned}$ | 0.11 min-1 | 100/-/60 | [10] |
| HC + PS | HC, Orifice plate | 43.8 | $\begin{aligned} & \mathrm{V}=10 \mathrm{~L}, \mathrm{P}=5 \mathrm{bar}, \mathrm{pH}=6, \\ & \mathrm{~T}=50^{\circ} \mathrm{C}, \mathrm{t}=2 \mathrm{~h}, \mathrm{PS}=0.7 \\ & \mathrm{mM} \end{aligned}$ | $\begin{aligned} & 12.6 \times \\ & 10-3 \mathrm{~min}-1 \end{aligned}$ | 81.3/-/ 76.9 | [9] |

## TEXT B

## Materials and Methods

## Chemicals and materials

Analytical grade chemicals, including BPA, ferrous sulfate $\left(\mathrm{FeSO}_{4} \cdot 7 \mathrm{H}_{2} \mathrm{O}\right)$, potassium peroxydisulfate (PS, $\mathrm{K}_{2} \mathrm{~S}_{2} \mathrm{O}_{8}$, CAS: 7727-21-1), sodium chloride $(\mathrm{NaCl})$, sodium sulfate $\left(\mathrm{Na}_{2} \mathrm{SO}_{4}\right)$, sodium hydrocarbonate $\left(\mathrm{NaHCO}_{3}\right)$, methyl alcohol $(\mathrm{MeOH})$, tert-butyl alcohol (TBA), were purchased from Aldrich, USA. The pH of the reaction mixtures was adjusted with 0.1 N NaOH and $0.1 \mathrm{~N} \mathrm{H}_{2} \mathrm{SO}_{4}$. A standard organic substance was also used (IHSS Suwannee river NOM RO Isolation 2R 101N) [14].

## Experimental setup

Figure S 1 shows the scheme of the experimental setup, which included: vertical multistage centrifugal pump (Grundfos CRNE-15), AC and HC generators, manometer and thermostat. The pump (1) sets the pressure of the circulating liquid, which enters the cavitation chamber (2) through a highpressure line. The cavitation chamber (Figure 1B) contains a titanium nozzle (outlet diameter 4 mm , internal diameter 10 mm , height 30 mm ) (2.1), and ultrasonic piezoceramic transducers diameter 2 cm (2.2) connected to 1.7 MHz sound generators (3) with a distance of 10 mm between the piezoelectric elements. The thermostat (4) with external cooling maintained a constant set temperature of $25^{\circ} \mathrm{C}$.


Fig. S 1. A - Laboratory bench for HC, AC and HAC generation; B - Cavitation chamber. 1 - vertical multistage pressure-controlled centrifugal pump, 2 - cavitation chamber, M - monometer, 2.1 - nozzle, 2.2 - piezo cells, 2.3 - cavitation cloud, 3 - high frequency generator $1.7 \mathrm{MHz}, 4$ - thermostat.

The total volume of the treated solution was 6.4 L . All elements of the reactor were made of stainless steel. The power consumption was 50 W for AC , and 400 W for HC (at 5 atm ). The power consumption was determined using an energy monitor (Voltcraft Energie Monitor 3000, Conrad Electronic SE, Germany, with an accuracy of $\pm 1 \%$ ).

## Experimental and analytic methods

For a typical degradation experiment, 6.4 L BPA aqueous solution with a concentration $43.8 \mu \mathrm{M}$ was prepared. In the HC experiments, the inlet pressure varied from 1.5 to 5 bar. In the AC only experiments, the solution was passed through an additional circuit bypassing the HC nozzle. In SRAOPs experiments, reagents were added to the cavitation chamber. The concentration of $\mathrm{K}_{2} \mathrm{~S}_{2} \mathrm{O}_{8}$ was set in the range of $219-657 \mu \mathrm{M}$, and $\mathrm{Fe}^{2+}$ in the range of $17.8-133.5 \mu \mathrm{M}$. Samples were taken from the cavitation chamber before the reaction ( 0 min , initial concentration), and after 5, 10, 20, 40, 60, 120, 180, 240 min reaction time. All experiments were performed in duplicates.

BPA was quantitatively analyzed by HPLC using an Agilent 1260 Infinity with Zorbax SB-C 18 $4.6 \times 150 \mathrm{~mm}$ column. Samples were filtered on FMPTFE- $0.45 \mu \mathrm{~m}$ membrane filters prior to analysis.

The degree of organic substrate mineralization was assessed by measuring the change in TOC, using a Shimadzu TOC-L CSN analyzer with a detection limit of $50 \mu \mathrm{~g} / \mathrm{L}$. Calibration of the analyzer was carried out using standard samples of potassium hydrophthalate and sodium hydrocarbonate.

The Multi 3410 Pocket Meter with SenTix®940 electrode (WTW, Germany) was used to measure pH values.

The toxicity assessment method used was based on bioluminescence inhibition of the recombinant strain of E. coli K12 TG1 carrying lux operons of the luminescent Photobacterium leiognathi [15]. The toxicity was tested before and after treatment for 240 min .

The degradation (E) and mineralization (M) of BPA were calculated by measuring the changes in BPA and TOC concentrations in the treated solution at time $\tau$ using the formulas:

$$
\begin{align*}
& E(\%)=\left(1-\frac{C_{\tau}}{C_{0}}\right) \times 100  \tag{1}\\
& M(\%)=\left(1-\frac{T O C_{\tau}}{T O C_{0}}\right) \times 100 \tag{2}
\end{align*}
$$

In our study, the synergy of $\mathrm{HAC} / \mathrm{PS} / \mathrm{Fe}^{2+}$ system was quantified by calculating synergistic indices $\varphi_{1}$ and $\varphi_{2}$ ( $\varphi>1$ indicates a synergistic effect). The synergistic indices for the efficiency of BPA degradation $\left(\varphi_{1}\right)$ and mineralization $\left(\varphi_{2}\right)$ were calculated according to the formulas:

$$
\begin{align*}
\varphi_{1} & =\frac{E_{H A C / \mathrm{PS} / \mathrm{Fe}^{2+}}}{E_{H A C / P S}+E_{P S / F e^{2+}}}  \tag{3}\\
\varphi_{2} & =\frac{\mathrm{M}_{H A C / \mathrm{PS} / \mathrm{Fe}^{2+}}}{\mathrm{M}_{H A C / P S}+\mathrm{M}_{P S / F e^{2+}}}, \tag{4}
\end{align*}
$$

where $E$ is the BPA degradation efficiency, $M$ is the mineralization efficiency (in terms of TOC decay). A similar calculation of synergistic indices was adopted analogously from the work of the authors A. Delavaran Shiraz et al. [16].


Fig. S 2. The kinetics of destruction and mineralization of BPA in hybrid $\mathrm{HAC} / \mathrm{PS} / \mathrm{Fe}^{2+}$ system at different molar ratio [BPA]: PS$] . \mathrm{C}_{0}(\mathrm{BPA})=43.8 \mu \mathrm{M}, \mathrm{C}_{0}\left(\mathrm{Fe}^{2+}\right)=89 \mu \mathrm{M}, \mathrm{C}_{0}(\mathrm{PS})=219,438$ и $657 \mu \mathrm{M}, \mathrm{T}=25 \pm 1^{\circ} \mathrm{C}, \mathrm{pH}=3.5$, $\mathrm{P}=5 \mathrm{~atm}$.

## References

[1] Torres R.A., Pétrier C., Combet E., Carrier M., et al. Ultrasonic cavitation applied to the treatment of bisphenol A. Effect of sonochemical parameters and analysis of BPA by-products. // Ultrasonics Sonochemistry 2008. Vol. 15, P. 605-611.
[2] Kitajima M., Hatanaka S., Hayashi S. Mechanism of O2-accelerated sonolysis of bisphenol A. // Ultrasonics 2006. Vol. 44, P. e371-e373.
[3] Deggelmann M., Nöpel J.-A., Rüdiger F., Paustian D., et al. Hydrodynamic cavitation for micropollutant degradation in water - Correlation of bisphenol A degradation with fluid mechanical properties. // Ultrasonics Sonochemistry 2022. Vol. 83, P. 105950.
[4] Lu G., Zhao L., Zhu M., Deng C., et al. Effect of Cavitation Hydrodynamic Parameters on Bisphenol A Removal. // Environmental Engineering Science Mary Ann Liebert, Inc., publishers, 2019. Vol. 36, P. 873-882.
[5] Dietrich M., Franke M., Stelter M., Braeutigam P. Degradation of endocrine disruptor bisphenol A by ultrasound-assisted electrochemical oxidation in water. // Ultrasonics Sonochemistry 2017. Vol. 39, P. 741-749.
[6] Ioan I., Wilson S., Lundanes E., Neculai A. Comparison of Fenton and sono-Fenton bisphenol A degradation. // Journal of Hazardous Materials 2007. Vol. 142, P. 559-563.
[7] Ghanbari F., Moradi M. Application of peroxymonosulfate and its activation methods for degradation of environmental organic pollutants: Review. // Chemical Engineering Journal 2017. Vol. 310,.
[8] Zhou Y., Gao Y., Pang S.-Y., Jiang J., et al. Oxidation of fluoroquinolone antibiotics by peroxymonosulfate without activation: Kinetics, products, and antibacterial deactivation. // Water Research 2018. Vol. 145, P. 210-219.
[9] Choi J., Cui M., Lee Y., Kim J., et al. Hydrodynamic cavitation and activated persulfate oxidation for degradation of bisphenol A: Kinetics and mechanism. // Chemical Engineering Journal 2018. Vol. 338, P. 323-332.
[10] Darsinou B., Frontistis Z., Antonopoulou M., Konstantinou I., et al. Sono-activated persulfate oxidation of bisphenol A: Kinetics, pathways and the controversial role of temperature. // Chemical Engineering Journal 2015. Vol. 280, P. 623-633.
[11] Torres R.A., Pétrier C., Combet E., Moulet F., et al. Bisphenol A Mineralization by Integrated Ultrasound-UV-Iron (II) Treatment. // Environmental Science \& Technology American Chemical Society, 2007. Vol. 41, P. 297-302.
[12] Chu J.-H., Kang J.-K., Park S.-J., Lee C.-G. Enhanced sonocatalytic degradation of bisphenol A with a magnetically recoverable biochar composite using rice husk and rice bran as substrate. // Journal of Environmental Chemical Engineering 2021. Vol. 9, P. 105284.
[13] Ryu B., Wong K. T., Choong C.E., Kim J.-R., et al. Degradation synergism between sonolysis and photocatalysis for organic pollutants with different hydrophobicity: A perspective of mechanism and application for high mineralization efficiency. // Journal of Hazardous Materials 2021. Vol. 416, P. 125787.
[14] Humic substances in the Suwannee River, Georgia; interactions, properties, and proposed structures. // Open-File Report / ed. Averett R. C. et al. 1989.
[15] Toxicological analysis. Method for determining the integral toxicity of surface water, including sea, ground, drinking and waste water, aqueous soil extracts, solid wastes and sewage sludge by measuring the intensity of bacterial bioluminescence of test-s. Moscow, 2010.
[16] Delavaran Shiraz A., Takdastan A., Mehbi Borghei S. Photo-Fenton like degradation of catechol using persulfate activated by UV and ferrous ions: Influencing operational parameters and feasibility studies // Journal of Molecular Liquids 2018. Vol. 249, P. 463-469.

