

# Emergence of superconductivity in mixture of nonsuperconducting ceramics $\text{La}_2\text{CuO}_4$ and $\text{La}_{1.56}\text{Sr}_{0.44}\text{CuO}_4$

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## Abstract.

Composite materials fabricated by annealing of nonsuperconducting ceramics  $\text{La}_2\text{CuO}_4$  and  $\text{La}_{1.56}\text{Sr}_{0.44}\text{CuO}_4$  at  $910^\circ\text{C}$  during various time are investigated. Areas of superconducting  $\text{La}_{1.85}\text{Sr}_{0.15}\text{CuO}_4$  phase arises at boundaries of contacting nonsuperconducting granules. The volume fraction of the superconducting phase increases with increasing the annealing time. A model describing the magnetic and transport properties of the samples at low magnetic fields is constructed. The magnetotransport characteristics of obtained samples at low magnetic fields ( $\sim 100$  Oe) are defined by a weak links network formed by superconducting areas. At high fields behavior of the system is defined by a magnetization of the disconnected superconducting islands. The average size of the superconducting areas has been estimated from an extended critical state model.

**Keywords:** magnetic properties, superconductivity, oxide superconductors, grain boundaries, LCO, LSCO, Josephson media

## 1. Introduction

The classical superconductor  $\text{La}_{2-x}\text{Sr}_x\text{CuO}_4$  (LSCO) is studied since 1986. Its concentration phase diagram is known in the entire range of  $x$  [1].  $\text{La}_2\text{CuO}_4$  (LCO) is a weak ferromagnetic with a Neel temperature  $T_N = 500$  K and it is dielectric. At  $x > 0.25$ ,  $\text{La}_{2-x}\text{Sr}_x\text{CuO}_4$  is a nonsuperconducting metal.

Recently [2,3], it was shown that an interface superconductivity arises on the boundary of LCO and  $\text{La}_{1.56}\text{Sr}_{0.44}\text{CuO}_4$  films. Study of such films is limited by the complexity of their synthesis (a layer-by-layer molecular beam epitaxy). A solid-phase synthesis does not require the complicated tools and is a simple method for obtaining superconducting materials with a different size of grains. In a mixture of the over- and under-doped precursors, the diffusion of doping atoms at boundaries between the granules occurs. The diffusion and parameters of the superconducting phase can be controlled by the annealing time  $t_a$ .

In this paper, we present the results of an experimental study of samples obtained by annealing the mixture of LCO and  $\text{La}_{1.56}\text{Sr}_{0.44}\text{CuO}_4$  ceramic powders. The synthesis of samples and the measuring techniques is described in Section 2. Experimental results are discussed in Section 3. A model describing the transport and the magnetic properties of the network of weak links is introduced in Section 4. Conclusions are presented in Section 5.

## 2. Materials and methods

The ceramic precursors of  $\text{La}_2\text{CuO}_4$  and  $\text{La}_{1.56}\text{Sr}_{0.44}\text{CuO}_4$  were synthesized by the standard solid-phase synthesis technique [4]. In addition, we synthesized the optimal doped sample LSCO as a benchmark. Then, the LCO and  $\text{La}_{1.56}\text{Sr}_{0.44}\text{CuO}_4$  powders were grounded in an agate mortar and mixed in 0.66 / 0.34 mass proportions. The selected proportion of the components would, with complete diffusion of the elements, compose the superconducting phase  $\text{La}_{1.85}\text{Sr}_{0.15}\text{CuO}_4$ . The mixture of LCO and  $\text{La}_{1.56}\text{Sr}_{0.44}\text{CuO}_4$  were annealed at  $T = 910^\circ\text{C}$  in a preheated oven. After annealing, for restoring an oxygen stoichiometry, the samples were slowly cooled with the same rate in an air atmosphere. The diffusion coefficient of oxygen in HTSC ceramics is tenfold higher than that of strontium cations [5]. Hence, this cooling almost did not affect the diffusion of strontium. A series of the samples was annealed during the time  $t_a = 2, 6, 20, 60, 200, 600, 2000, 6000, 20000$  min.

Scanning electron microscopy of the samples was performed on microscope Hitachi TM 3000. Temperature dependencies of the resistance  $R(T)$  were measured by four-probe method by using QDS device of PPMS-6000. Samples with the parallelepiped form had dimensions of about  $1 \times 1 \times 10 \text{ mm}^3$ . Transport current was equal to 1 mA. The temperature dependencies of the magnetization  $M(T)$  and the magnetic field dependencies of the magnetization  $M(H)$  were performed by using QD PPMS-6000 magnetometer.

### 3. Results and discussion

Fig. 1 shows microphotographs of samples with  $t_a = 2$  and 2000 min. All the samples consist from irregular granules. The average granule size are estimated from microphotographs as  $1.1 \pm 0.1$ ,  $1.2 \pm 0.1$ ,  $1.3 \pm 0.1 \text{ }\mu\text{m}$  for  $t_a = 20, 200, 2000 \text{ min}$ .

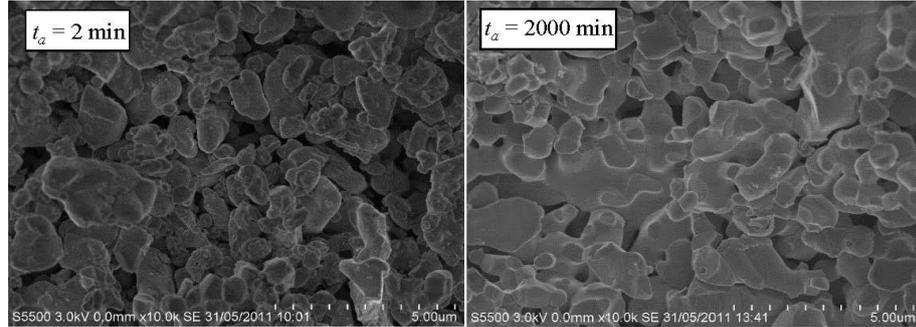


Fig. 1. Microphotographs of the samples with the annealing time  $t_a = 2$  and 2000 min.

Fig. 2a shows temperature dependencies of the resistance of samples with different annealing times. All samples demonstrate a resistance jump at  $T_c = 37.5 \text{ K}$ , the critical temperature of the optimally doped LSCO. For the samples with  $t_a = 6$  and 20 min the resistance reaches the minimum at  $T < T_c$  and then grows as temperature decreases. For the samples with longer  $t_a$  the resistance decreases at  $T < T_c$  with decreasing temperature. Only for the sample with  $t_a = 20000 \text{ min}$  the  $R(T)$  curve reaches  $R = 0$ . At any fixed temperature the resistance decreases as the annealing time  $t_a$  increases. These facts indicate that there is the optimally doped LSCO in the samples and the volume fraction of the superconducting phase in the samples increases with  $t_a$ .

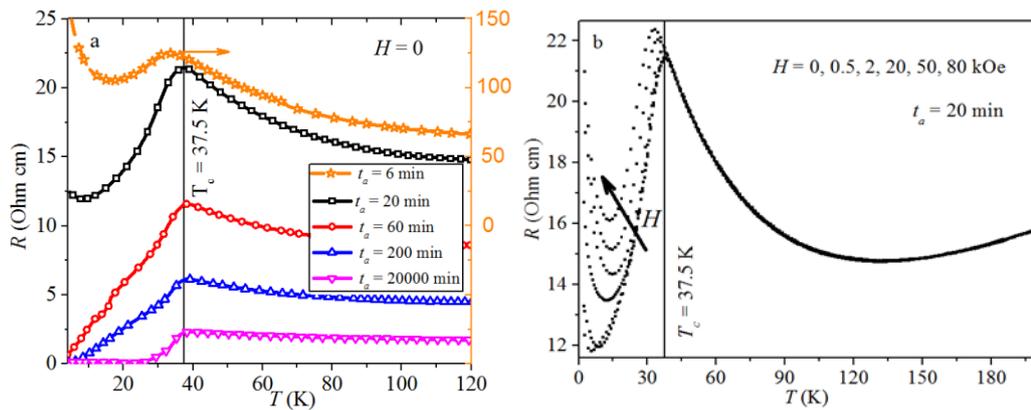


Fig. 2. Temperature dependencies of the resistance of samples with different annealing time  $t_a$  (a) and the dependencies for  $t_a = 20 \text{ min}$  in magnetic fields (b).

Fig. 2b demonstrates temperature dependencies of the resistance for the sample with  $t_a = 20 \text{ min}$  in various external magnetic fields. Influence of the magnetic field on the resistance of the samples is clearly pronounced in Fig. 3. It shows the dependencies of the additional resistance  $\Delta R(T) = R(T, H) - R(T, H = 0)$ . In high fields ( $H = 20, 80 \text{ kOe}$ ) the  $\Delta R(T)$  dependencies have a knee. This knee shifts to lower temperatures as the field is increased. These dependencies look similar to the  $\Delta R(T)$  dependencies of polycrystalline superconducting composites [6-8] representing a network of Josephson weak links. For the composites the knee indicates that the superconductivity is suppressed in the surface of superconducting areas.

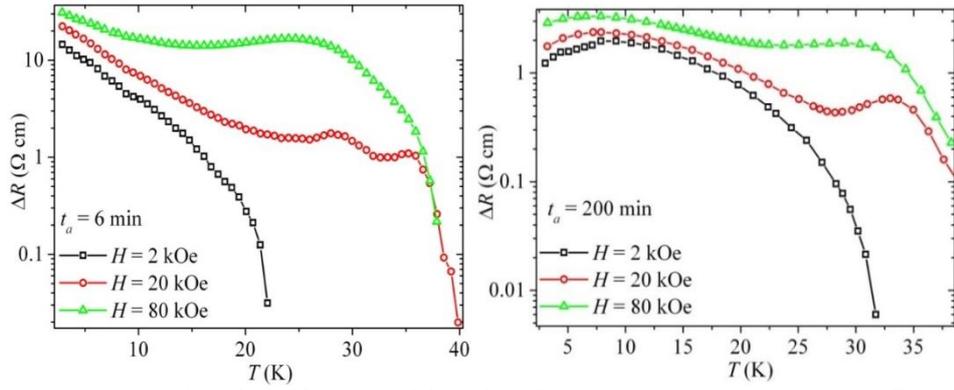


Fig. 3. Temperature dependencies of the additional resistance  $\Delta R(T) = R(T, H) - R(T, H = 0)$  for  $t_a = 6$  and 200 min.

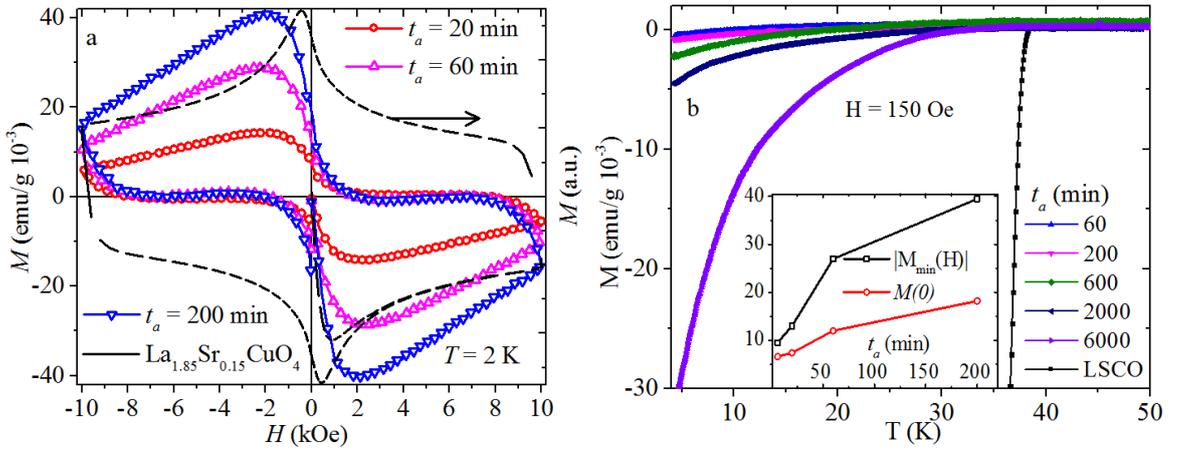


Fig. 4. Dependencies of the magnetization  $M$  on the magnetic field  $H$  (a) and temperature dependencies of the magnetization  $M(T)$  in the ZFC regime (b). Insert shows the trapped field  $M(0)$  and the absolute value of the magnetization minimum  $|M_{\min}|$ .

Magnetization hysteresis curves of the samples are typical for HTSC. Also there is an additional paramagnetic contribution, which is apparently provided by the LCO granules. The  $M(H)$  dependencies are shown on Fig. 4a (the paramagnetic contribution is subtracted for these loops). The  $M(H)$  dependence of the optimally doped LSCO is also presented here. The magnetization loops of the samples are asymmetric relative to the  $M = 0$  axis. Fig. 4b shows temperature dependencies of the magnetization  $M(T)$  for some samples. The  $M(T)$  dependencies tend to zero at  $T_c = 37.5$  K. This, as well as the values of  $T_c$  obtained from  $R(T)$ , indicates that there is the optimally doped LSCO in the samples. The inset shows the dependencies of trapped field  $M(0)$  and the minimum of the magnetization  $|M_{\min}|$  on  $t_a$ . The  $M(0)$  and  $|M_{\min}|$  values, as well as magnetization width  $\Delta M$ , depend on the volume of the superconducting phase. The observed growth of these parameters is supported to be due to the increasing of the superconducting volume fraction in the samples with  $t_a$ .

According to the extended critical state model (ECSM) [9, 10], an asymmetry of the magnetization loops and the trapped field  $M(0)$  depend on the relation between the size of the current circulation  $d$  and the depth of the surface layer  $l_s$ . Also the critical current density  $J_c$  depends on the  $d/l_s$  ratio. From ECSM it follows that  $J_c \approx J_{cb}(1 - 2l_s/d)^3$ , where  $J_{cb}$  is the critical current density of the sample with  $d \gg l_s$  [11]. This relation allows us to estimate the  $d/l_s$  ratio from the observed asymmetry of magnetization loops. The critical current density  $J_c$  is given by the Bean formula  $J_c = \Delta M/k$ , where  $\Delta M$  is the irreversible magnetization,  $\Delta M = M_d - M_{\text{up}}$ ,  $M_d(H)$  is the magnetization branch for the decreasing field,  $M_{\text{up}}(H)$  is the magnetization branch for the increasing field, a parameter  $k$  is determined by the sample geometry and has the length dimension. For the polycrystalline sample one can use  $k = d/3$  (in SI units) [12]. For the samples with  $d \gg l_s$ , the

magnetization loop is symmetric relative to the  $M = 0$  axis, and the irreversible magnetization  $\Delta M$  equals  $2|M_{\text{up}}|$  at the wide field range. Given  $J_{cb} \approx (2|M_{\text{up}}|)/k$  we obtain  $d/l_s \approx 2 / (1 - (\Delta M/2/M_{\text{up}}))^{1/3}$ .

We assume that  $d$  corresponds to an average size of the superconducting areas in the investigated samples. Results of the estimations of  $d/l_s$  are presented in Table 1 for the values of  $\Delta M$  and  $M_{\text{up}}$  at  $H = 4000$  Oe. This field is about the full penetration field of the investigated samples.

$t_a$ , min	$d/l_s$	$I_c$ , $\mu\text{A}$
20000	-	18.5
200	$8.6 \pm 0.8$	3
60	$8.5 \pm 0.7$	2.2
20	$9.0 \pm 0.9$	2
6	$10.7 \pm 1.3$	1
LSCO	$43.3 \pm 3.3$	-

Table 1. Estimated parameters: the  $d/l_s$  ratio and the critical current  $I_c$ .

Given the average size of the benchmark LSCO granules to equal  $\sim 5\text{-}10 \mu\text{m}$ , the averaged island size  $d$  was supposed to be not higher than  $\sim 1 \mu\text{m}$  for all  $t_a$ . Assuming the value of  $l_s$  does not change with  $t_a$ , the size  $d$  is resulted to be independent of  $t_a$  within the errors. This is an unusual result because the volume fraction of the superconducting phase is found to grow with  $t_a$ .

Basing on experimental data we suppose that superconducting islands arise at boundaries of contacting granules as a result of strontium diffusion from over- to under-doped granules during the annealing. The stationary of the size  $d$  is an indirect confirmation of the diffusion mechanism of formation of the superconducting phase. When an over-doped granule contacts with an under-doped one, the impurities redistribute during the annealing. The redistribution forms a diffusion front [13] with the fixed depth. In this front, the strontium concentration is optimal for the superconducting phase. Before the front, the strontium concentration is insufficient, behind the concentration is exceeded. The depth of this front is resulted to be the size of the superconducting island.

We suggest that two superconducting subsystems [12] are segregated in the investigated samples. The first is superconducting islands emerged between granules with different Sr contents. The second is a network of weak links formed inside and between the superconducting areas. These subsystems demonstrate different behavior in magnetic fields and temperatures as well as for polycrystalline superconductors [6, 14]. At a low magnetic field (smaller than  $\sim 100$  Oe), the critical current of the samples is defined by the weak links network. The thermally activated phase slippage model (TAPS) [15] is used to describe the long transition below  $T_c$  on the  $R(T)$  dependencies of polycrystalline superconductors [16]. The average critical current  $I$  of weak links is used as the fitting parameter of TAPS. The TAPS curve for  $I_c = 18.2 \pm 1.5 \mu\text{A}$  coincides with the  $R(T)$  dependence of the sample with  $t_a = 20000$  min. The  $R(T)$  dependencies of other samples are fitted worse. Agreement can be improved by taking into account i) the distribution function of the critical currents in weak links networks and ii) the temperature dependence of the resistance. By using approximate TAPS estimations of the averaged critical current without complicating accountings, we find that  $I_c$  grows with increasing  $t_a$  (Table 1).

At higher fields ( $H > 100$  Oe) the weak links are resistive, and nondissipative supercurrents flow only into isolated superconducting islands. At  $H$  greater than  $\sim 10$  kOe these islands contribute observably in the resistivity of the samples. It is because the magnetic field suppresses the superconductivity in the surface regions of the islands. The depth of the resistive surface region  $l_s$  grows as the magnetic field increases.

The number of the superconducting islands increases, as well as the critical current of the network, with increasing of the annealing time  $t_a$ . However, even at the longest  $t_a$ , total diffusion of strontium does not occur. The inner volume of the granules remains nonsuperconducting.

#### 4. Theory

Now a model of the weak links network is described. This model gives the behavior of the samples in low fields ( $H \sim 100$  Oe). We consider the two-dimensional task and do not account any temperature dependencies. Nonsuperconducting granules were placed in the cells of a disordered square lattice with size  $N \times N$  on the  $x$ - $y$  plane (Fig. 5a). The size of the granules along the  $z$ -axis is considered to be infinite. During annealing, granules contact better one to other and the superconducting areas emerge at the boundaries of the granules. The areas build a Josephson weak links network. In our model, the superconducting islands occur in some edges of cells. The shape of the superconducting areas is not important. We state that each superconducting area includes only one Josephson junction (Fig. 5b). Several weak links can occur on the superconducting area. But only the links with the minimal critical current determines the properties of superconducting circuits. Therefore this simplification does not affect the simulation of the electromagnetic properties of the network.

New superconducting edges are appeared during the annealing. These edges with Josephson junctions form closed contours around the normal phase clusters (Fig. 5c). Such the contours are the centers of pinning for the magnetic flux. The number of the contours and their size distribution determine the electromagnetic properties of the whole system.

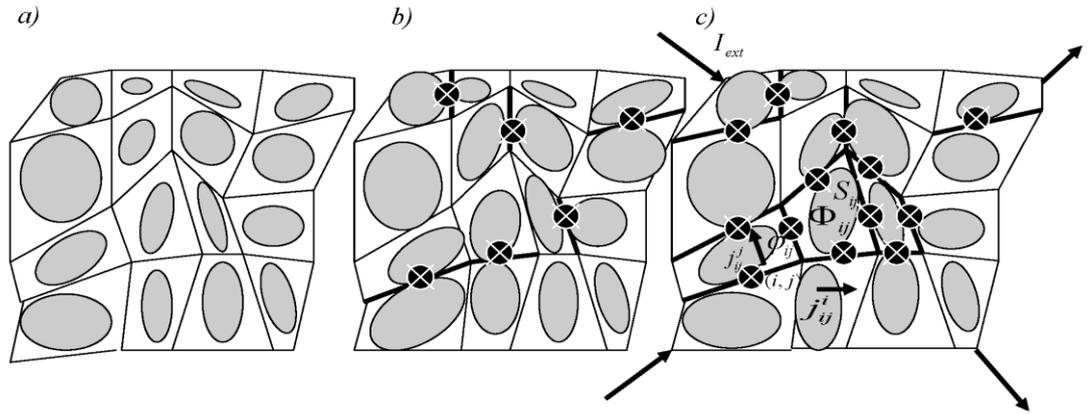


Fig. 5. The scheme of the weak links network formed by annealing.  $t_a$  increases from left to right, bold lines indicate the superconducting boundaries, crossed circles are the Josephson junctions.

Each Josephson junction is characterized by a dynamic variable, which is the gauge-invariant phase difference. Let us denote it as  $\varphi_{i,j}$  for the junctions in the "vertical" edges of cells and  $\theta_{i,j}$  for the "horizontal" ones (Fig. 5). The grid cells are numbered from the lower left corner. The density of the "vertical" and the "horizontal" currents, the cell area  $S_{ij}$  and the magnetic flux  $\Phi_{ij}$  through the cell are given in Fig. 5 also. For  $j_{i,j}^i$  and  $j_{i,j}^j$ , a discrete analog of Maxwell's equations is written

$$\begin{aligned} 4\pi j_{i,j}^i &= \frac{H_{i,j} - H_{i,j-1}}{d}; & 4\pi j_{i,1}^i &= \frac{H_{i,1} - H_{ext}}{d}; & 4\pi j_{i,N}^i &= \frac{H_{ext} - H_{i,N-1}}{d} \\ 4\pi j_{i,j}^j &= \frac{H_{i,j-1} - H_{i,j}}{d}; & 4\pi j_{1,j}^j &= \frac{H_{ext} - H_{1,j}}{d}; & 4\pi j_{N,j}^j &= \frac{H_{N-1,j} - H_{ext}}{d} \end{aligned} \quad (1)$$

where  $H_{i,j}$  is the magnetic field in the  $ij$ -th cell of the system,  $d$  is the length of the cell edge. This length is equal to the average size of the superconducting islands that is estimated above. From the resistive model of the Josephson junction [17], the junction current consists of normal and superconducting components:

$$\begin{aligned} j_{i,j}^i &= \frac{\Phi_0}{2\pi r} \frac{d\theta_{i,j}}{dt} + j_{ci,j}^i \sin \theta_{i,j} \\ j_{i,j}^j &= \frac{\Phi_0}{2\pi r} \frac{d\varphi_{i,j}}{dt} + j_{ci,j}^j \sin \varphi_{i,j} \end{aligned} \quad (2)$$

where  $r$  is the normal resistance of the junction and  $j_{ci,j}^{i(j)}$  is its critical current density. The magnetic

$$j_{ci,j}^{i(j)}$$

flux through the cell is expressed as [18]:

$$\Phi_{i,j} = \frac{\Phi_0}{2\pi} (\varphi_{i,j} + \theta_{i,j+1} - \varphi_{i+1,j} - \theta_{i,j}) \quad (3)$$

Combining (1) - (3), we obtain a system of equations for  $\varphi_{i,j}$  and  $\theta_{i,j}$  in the dimensionless form [19]:

$$\begin{aligned} \tau \frac{d\theta_{i,j}}{dt} + V \sin \theta_{i,j} &= s_{i,j} (\varphi_{i,j} + \theta_{i,j+1} - \varphi_{i+1,j} - \theta_{i,j}) - s_{i,j-1} (\varphi_{i,j-1} + \theta_{i,j} - \varphi_{i+1,j-1} - \theta_{i,j-1}) \\ \tau \frac{d\varphi_{i,j}}{dt} + V \sin \varphi_{i,j} &= s_{i,j-1} (\varphi_{i,j-1} + \theta_{i,j} - \varphi_{i+1,j-1} - \theta_{i,j-1}) - s_{i,j} (\varphi_{i,j} + \theta_{i,j+1} - \varphi_{i+1,j} - \theta_{i,j}) \\ \tau &= \frac{4\pi \langle S_{ij} \rangle d}{r}; \quad V = \frac{8\pi^2 d \langle S_{ij} \rangle j_{ci,j}^{i(j)}}{\Phi_0}; \quad s_{i,j} = \frac{\langle S_{i,j} \rangle}{S_{i,j}}; \quad (4) \end{aligned}$$

where  $\Phi_0$  is the magnetic flux quantum and  $S_{i,j}$  is the area of the cell. For the boundary junctions, according to (1),  $H_{i,j}$  is replaced by  $H_{ext}$  in (4). For example, at the upper boundary, it is resulted in

$$\tau \frac{d\theta_{1,j}}{dt} + V \sin \theta_{1,j} = s_{1,j} (\varphi_{1,j} + \theta_{1,j+1} - \varphi_{2,j} - \theta_{1,j}) - 2\pi h_{ext}; \quad h_{ext} = \frac{H_{ext} \langle S_{i,j} \rangle}{\Phi_0} \quad (5)$$

The system parameter  $V_{ij}^{i(j)}$  depends on the critical current of the junctions. This value concerns to a number of magnetic vortices in the corresponding contour. If some edge of cells does not contain the superconducting island and the Josephson junction then its critical current and the quantity  $V_{ij}^{i(j)}$  are equal to zero. When all  $V_{ij}^{i(j)} \gg 1$ , the system has a large number of metastable energy states. Consequently, the network demonstrates the hysteresis magnetic behavior. In the contrary case of all  $V_{ij}^{i(j)} \ll 1$ , the magnetic dynamics of the network is reversible [18]. Using estimated values (of  $d$  and  $I_c$ ) the averaged  $\langle V \rangle$  is found to be  $\sim 40$ .

In our model, we take into account the changes that occur with the sample during the annealing. Initially, all the granules are considered to be not touched one to other and all values  $V_{ij}^{i(j)}$  equal zero. As  $t_a$  increases, the granules begin to touch some nearest neighbors. The edge of the lattice cell, along which the granules come into contact, becomes superconducting. We introduce the quantity  $a$  determining the probability of arising of the new superconducting edges during the time cycle. Then the number of the superconducting edges is determined by  $t_a$  and  $a$ . During annealing, the amount of the superconducting edges increases and the closed superconducting contours are formed. The normal clusters surrounded by the superconducting contours are the pinning centers. The results of  $21 \times 21$  lattice modeling for the probability  $a = 0.01$  are presented in Fig. 6. It is seen that, the pinning centers in the system are added as  $t_a$  increases.

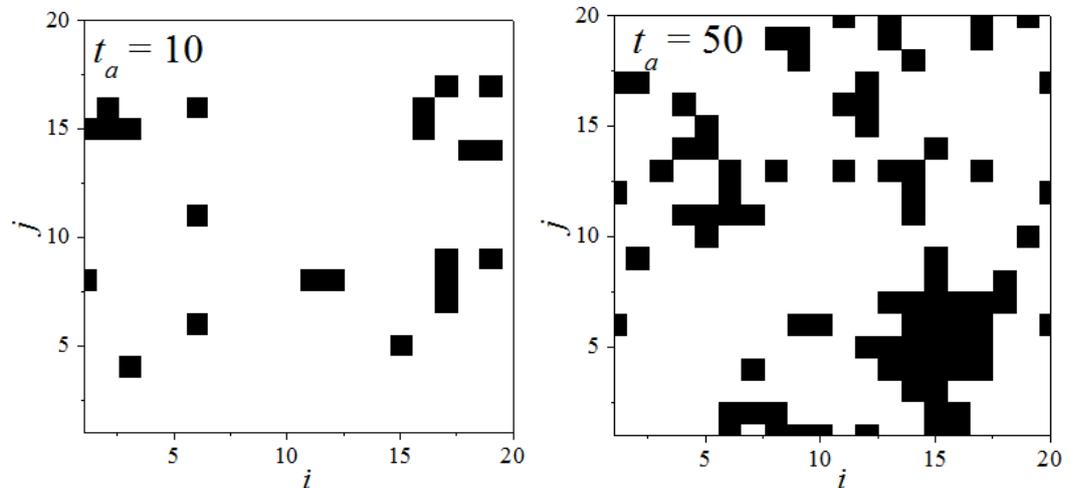


Fig. 6. Simulation results. Black sections denote pinning centers (the normal clusters, surrounded by the closed superconducting contour).

We simulate the behavior of the annealed sample in two modes. The first correspond to the external magnetic field  $H_{ext}(t)$  applied along the  $z$ -axis of the sample. The second correspond to the direct current  $I_{ext}$  along the  $x$ -axis of the sample. In this geometry, the demagnetization factor can be neglected.

In the first case, the critical current density depends on magnetic field as  $j_{ci,j}^{(i)} = j_{ci,j}^{(j)} / (1 + H_{ij}/H_0)$ . The values of  $j_{ci,j}^{(i)}$  are chosen to obtain  $V = 40$ . It does not matter whether the critical currents of all the junctions are different or identical. The electromagnetic properties of the system are determined only by the mean value of the critical current. The external field is changed so that its dimensionless value is added by one  $h_{ext} \rightarrow h_{ext} + 1$  during the computational cycle. This field growth is assumed to be so slow that all the processes in the system could be completed before the next cycle. For each value of the external field, we calculate the dimensionless mean value of the magnetic field inside the sample and the magnetization:

$$b = \frac{1}{N^2} \sum_{i,j} \frac{\Phi_{i,j}}{\Phi_0} s_{i,j}; \quad (5)$$

$$M = \frac{1}{4\pi} (b - h_{ext})$$

As a result, the magnetization loops for various  $t_a$  were computed (Fig. 7a). Here the cell areas are chosen to be the same and, consequently,  $S_{i,j} = 1$  for all cells of the system. It is seen that the trapped magnetic flux increases with  $t_a$  as well as the  $M(0)$  values. This result qualitatively agrees with the experiments. The shape of the hysteresis loop is affected by the value of  $H_0$ , which depends on the material.

In the second case, a direct current  $I_{ext}$  flow through the network without external magnetic field. We assume that the current is injected into the "horizontal" contacts of the upper and lower boundaries of the system (Fig. 5c). Then, the boundary conditions of (4) are changed. At the upper and lower boundaries, the external magnetic field is replaced by  $i_{ext} = I_{ext} dS / \Phi_0$ . At the right and left boundaries, the external field is replaced by zero. Now  $V$  is considered to be independent of the local magnetic field. The values of  $j_{ci,j}^{(i)}$  are chosen to have  $V = 40$ . Further, the average voltage for horizontal contacts was calculated for various  $I_{ext}$  by the formula:

$$u^i = \frac{1}{N(N-1)} \frac{2\pi j_{ci,j}}{\Phi_0} \sum_{i,j} u_{i,j}^i$$

$$u_{i,j}^i = \frac{\Phi_0}{2\pi} \frac{d\theta_{i,j}}{dt}$$

The  $u^i(2\pi i_{ext}/V)$  dependencies for different  $t_a$  are presented in Fig. 7b. It is seen that for higher  $t_a$ , the voltage-current curve is closer to the curve of a superconductor with  $j_c = V/2\pi$ . The increase of  $u^i$  is caused by the increasing number of the superconducting contours, which are able to carry the corresponding critical current.

The dependence of the resistance on the external magnetic field  $R(H)$  is computed also (Fig. 7c). The external current  $i_{ext} = 0.9(V/2\pi)$  flow through the sample according to the scheme in Fig. 5c. The dependence of  $j_c$  on the external magnetic field is given by  $j_c = j_{c0} / (1 + H_{ij}/H_0)$  with  $H_0 = 2$ . Fig. 7c shows, the resistance of all samples increases with  $h$  until the critical field of weak links. The critical field of weak links depends on the parameter  $H_0$ . It is also seen that the resistance decreases with increasing  $t_a$ . The computed  $R(H)$  dependencies qualitatively coincide with experimental curves of polycrystalline superconductors in low fields [6-8].

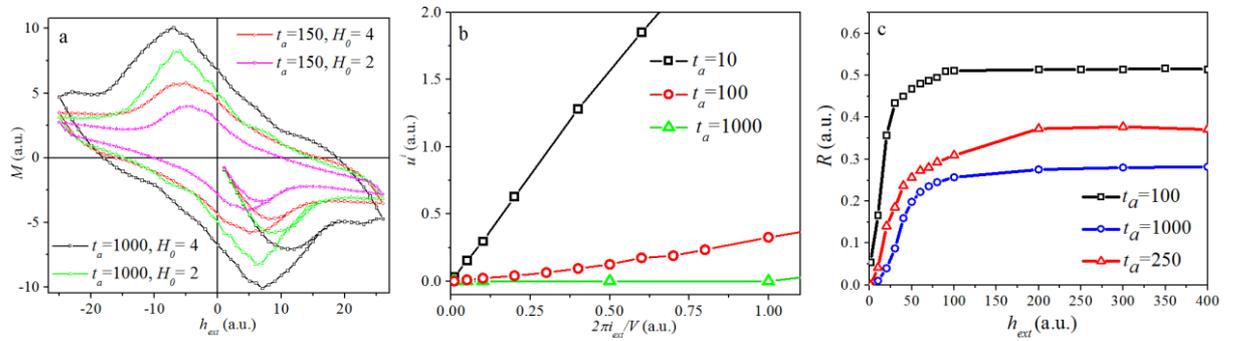


Fig. 7. Computed curves for some  $t_a$ : magnetization loops with different  $H_0$  (a),  $I$ - $V$  curves (b), the resistance  $R$  versus the external magnetic field  $H$  (c).

## 5. Conclusions

Annealing the mixture of powders of nonsuperconducting ceramics  $\text{La}_2\text{CuO}_4$  and  $\text{La}_{1.56}\text{Sr}_{0.44}\text{CuO}_4$  we have obtained the composite samples owning superconducting properties. From the results of experimental investigations and numerical simulating we can conclude:

1. The volume fraction of the superconducting phase increases with annealing time  $t_a$ . However, even at the longest  $t_a$ , the fraction of superconducting phase is smaller than 50 %. Consequently, complete diffusion of strontium does not occur. The superconducting phase in the samples is the islands of LSCO at the boundaries of the contacting over- and under-doped granules. The inner bulk of the granules remains nonsuperconducting.

2. The behavior of the samples in low ( $< 100$  Oe) magnetic fields is determined by the properties of the weak links network. At high magnetic field, the superconductivity of weak links is destroyed. Then the behavior of the system is determined by separate LSCO islands. Superconductivity is suppressed by magnetic field in the surface regions of the superconducting islands. This contribution to resistance is significant at magnetic fields higher than 10 kOe.

3. The extended critical state model is used to estimate the average size  $d$  of the superconducting islands. It is shown that  $d$  does not depend on  $t_a$ . This confirms the diffusion formation of the superconducting islands.

4. The model of the magnetic and transport behavior of the samples in low magnetic fields is presented. The model adequately describes the observed physical properties of the samples. In addition, the model predicts the possibility to discover some new interesting phenomena that can realize in our system, for example, self-organized criticality [19].

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